

Where Innovation Never Stops

Practical Guide Shoulder Milling



BEAN
HM390 FTD D063-05-27-19
T=9 N·M

Overview - Radially Clamped 90° Shoulder Milling Systems

The **allrounder** - insert selection

HELI3MILL
HM390 LINE



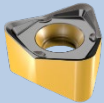
3 cutting edges

Smooth cut



The **economical** radial insert

HELI DO
690 LINE



6 cutting edges

Smooth cut



The **specialist** for long overhangs

HELI DO
690 LINE

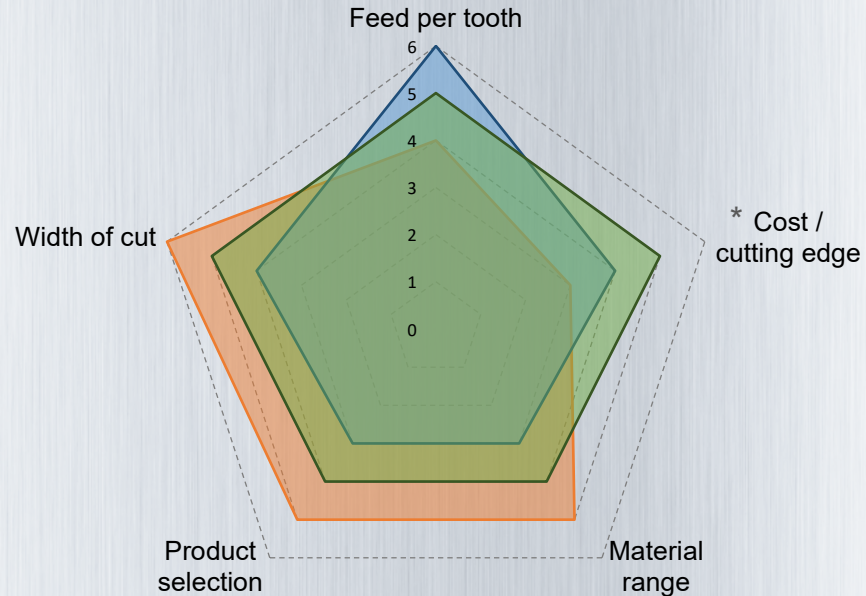


6 cutting edges

Smooth cut



System features

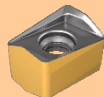


*
6 = low costs
1 = high costs

Supplementary Systems for Shoulder Milling

The **hard working** tool

HELIDO
490 LINE



4 cutting edges

Smooth cut

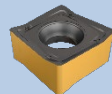


The **powerful** option

HELIDO NEODO
890 LINE S90° LINE



90° lead angle



88° lead angle

Smooth cut



The **noiseless** specialist

Specialist eliminating vibrations by unique Kordelverzahnung

MILLSHRED
P290 LINE

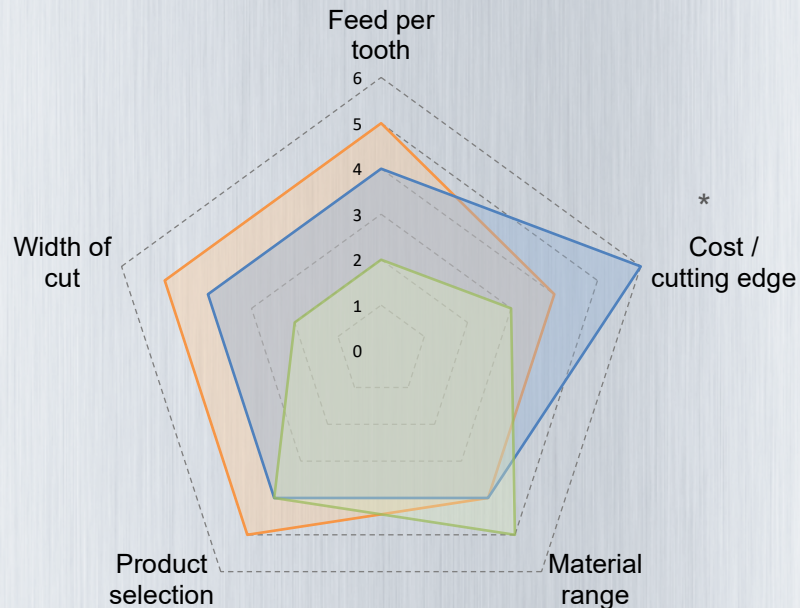


2 cutting edges

Smooth cut



System features



*
6 = low costs
1 = high costs

Overview - Tangentially Clamped 90° Shoulder Milling Inserts

The **productivity** booster

HELITANG
T490 LINE



4 cutting edges

Smooth cut *



* in relation to tangential tools

The **economical** tangential insert

LOGIQ8TANG
T890 MILLING LINE

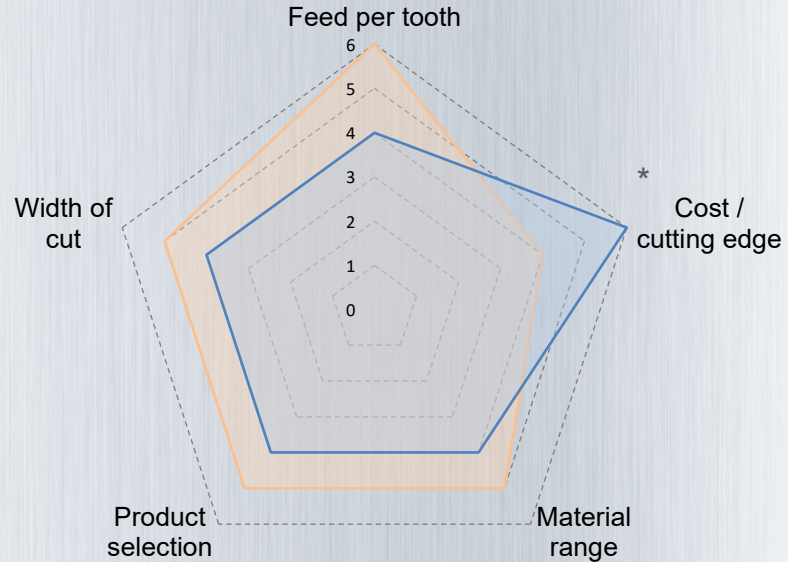


8 cutting edges

Smooth cut

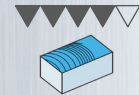
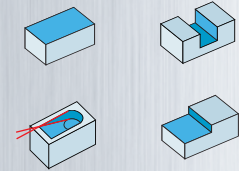


System features



*
6 = low costs
1 = high costs

- ✓ Positive, single-sided inserts with 3 cutting edges
- ✓ Very easy cut, first choice for ISO-M / S
- ✓ Effective and precise machining of 90° shoulders
- ✓ For roughing and finishing operations
- ✓ Flexible use for ISO P / M / K / N / S



Product selection / chip formers / cutting grades

- End mills: Ø 6 – 50 mm *HM390 E__*
- Shell mills: Ø 32 – 200 mm *HM390 F__*
- Connections: shank / arbor / Camfix / MM / Flexfit
- Pitch: coarse and fine pitch / each with internal coolant
- Insert sizes [mm]: 04 / 05 / 07 / 10 / 15 / 19
- Insert corner radii [mm]: 0.2 / 0.4 / 0.8 / 1.0 / 1.2 / 1.6 / 2.0 / 2.4 / 3.2 / 4.0
- Insert designs: ground = *HM390 T_C_* // pressed = *HM390 T_K_*

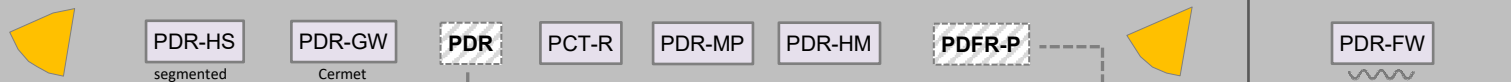


**Recommended
 chip formers & cutting
 grades**

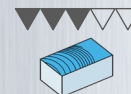
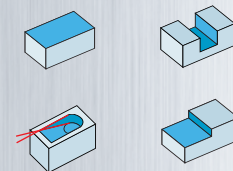
For ISO-S / M / N materials
 we recommend ground
 insert options.

stable → super positive

Shred profile



- ✓ Double-sided insert
- ✓ 6 right-hand cutting edges
- ✓ Smooth cut
- ✓ Economical 90° face milling
- ✓ Semifinishing / roughing



**Recommended
chip formers &
cutting grades**

For ISO-S / M we recommend ground insert options.

Product selection / chip formers / cutting grades

- End mills: \varnothing 18 – 40 mm *H690 E*__
- Shell mills: \varnothing 40 – 125 mm *H690 F*__
- Connections: shank / arbor
- Pitch: coarse, regular / each with internal coolant
- Insert sizes [mm]: 04 / 07
- Insert corner radii [mm]: 0.8 / 1.2 / 1.6 / 2.0
- Insert designs: ground = *H690 WNHU*_ // pressed = *H690 WNMU*_

stable → super positive



P

IC5400/5600 IC330

IC808

IC830 / IC845

10 30 50

K

IC5100

IC810

IC808

10 30 50

M/S

IC808

IC830 / IC 330

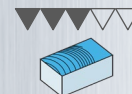
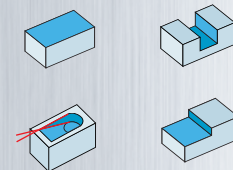
IC840 / IC882

10 30 50

N

10 30

- ✓ 6 double-sided, right-hand cutting edges
- ✓ Low impact of axial forces on component
- ✓ For long overhangs
- ✓ Less vibrations
- ✓ Economical shoulder milling



Product selection / chip formers / cutting grades

- End mills: \varnothing 32 – 40 mm *H690 E...R10 / R16*
- Shell mills: \varnothing 40 – 160 mm *H690 F...R10 / R16*
- Connection: shank / arbor
- Pitch: coarse, regular / each with internal coolant
- Insert sizes [mm]: 10 / 16
- Insert corner radii [mm]: 0.4 / 0.8 / 1.0
- Insert designs: ground = *H690 TNCX_* // pressed = *H690 TNKX_*

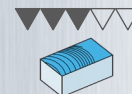
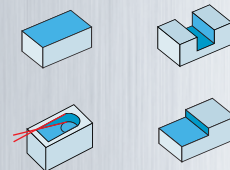
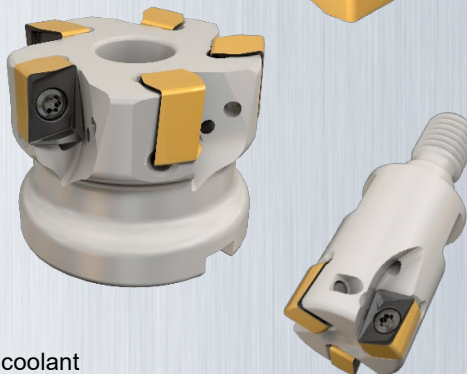
Recommended chip formers & cutting grades

For ISO-S / M materials we recommend ground insert options.

stable super positive chip splitter



- ✓ Best productivity with double-sided insert
- ✓ Option instead of tangential milling systems
- ✓ Roughing geometries
- ✓ For large cutting widths



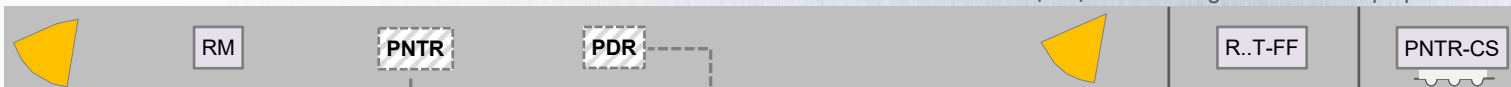
**Recommended
chip formers &
cutting grades**

For ISO-S / M materials
we recommend ground
insert options.

Product selection / chip formers / cutting grades

- End mills: \varnothing 16 – 32 mm [H490 E90A_](#)
- Shell mills: \varnothing 32 – 250 mm [H490 F90A_](#)
- Extended flute shell mill: \varnothing 50 – 80 mm [H490 SM_](#)
- Connections: shank / arbor
- Pitch: coarse, regular / each with internal coolant
- Insert sizes [mm]: 09 / 12 / 17
- Insert corner radii [mm]: 0.4 / 0.8 / 1.2 / 1.6 / 2.0 / 2.4
- Insert designs: ground = [H490 ANCX_](#) // pressed = [H490 ANKX_](#)

stable —————→ super positive High feed chip splitter



P

IC5400	IC330
IC808	
IC830 / IC845	

10 30 50

K

IC5100
IC810
IC808

10 30 50

M/S

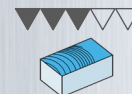
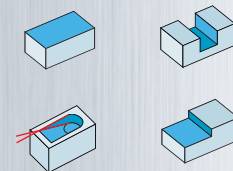
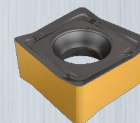
IC808
IC830 / IC330

10 30 50

N

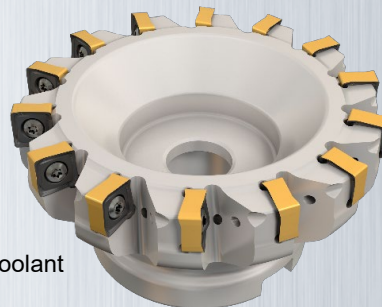
10 30

- ✓ 8 right-hand or 8 left-hand cutting edges
- ✓ Most attractive price per cutting edge
- ✓ Option instead of face milling
- ✓ Ideal for special solutions



Product selection / chip formers / cutting grades

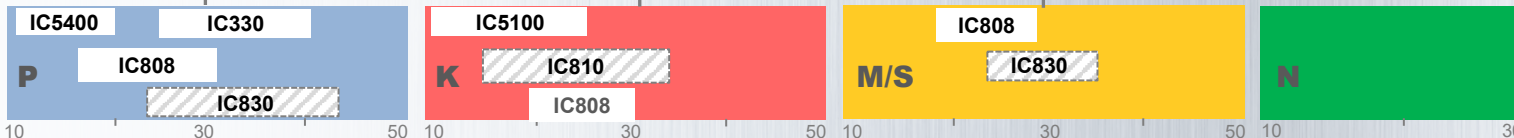
- Shell mills: \varnothing 40 – 160 mm [S890 FSN_](#)
- Slotting cutters: \varnothing 125 mm [S890 SSB_](#)
- Connection: arbor type A or B
- Pitch: coarse, regular / each with internal coolant
- Insert sizes [mm]: 13
- Insert corner radii [mm]: 0.8
- Insert designs: ground = [S890 SNHU_](#) // pressed = [S890 SNMU_](#)
Finishing insert



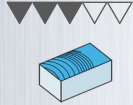
**Recommended
chip formers &
cutting grades**

For ISO-S / M materials we recommend ground insert options.

stable → super positive



- ✓ 8 right-hand cutting edges
- ✓ very high Productivity
- ✓ carefree handling
- ✓ High process machining stability

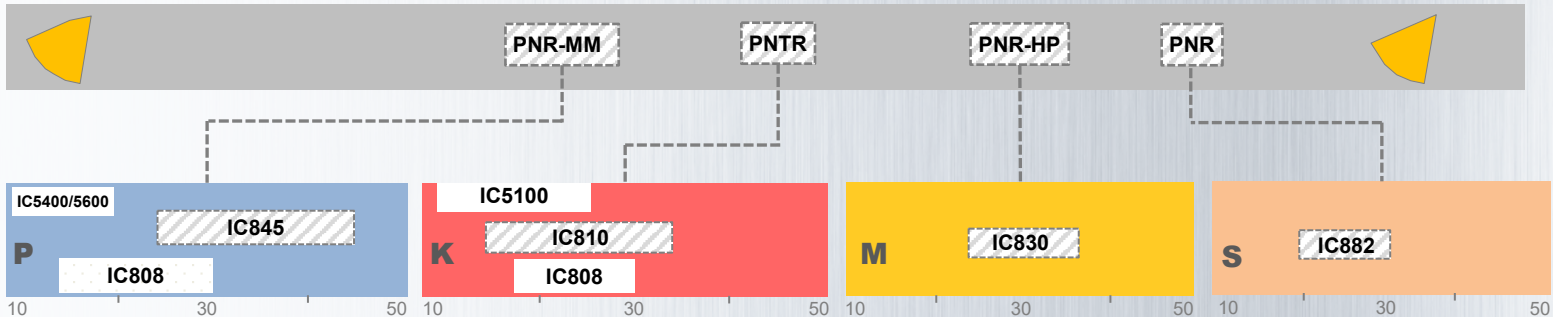


**Recommended
chip formers &
cutting grades**

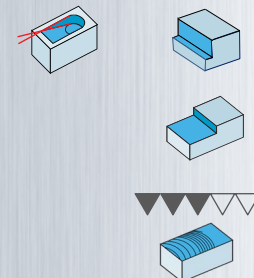
Product selection / chip formers / cutting grades

- End mills: \varnothing 25 – 32 mm *S890 E*__
- Shell mills: \varnothing 40 – 125 mm *S890 F*__
- Connection: arbor type A or B
- Pitch: regular / fine , each with internal coolant
- Insert sizes [mm]: 08
- Insert corner radii [mm]: 0,8 / 1,2
- Insert designs: pressed *S890 SZMU 0804..._* ground = *S890 SZHU_*

stable → super positiv

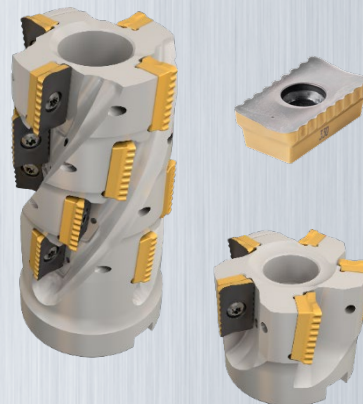


- ✓ Single-sided, positive insert
- ✓ Best solution to eliminate vibrations
- ✓ Low cutting forces, less bending forces
- ✓ For long overhangs
- ✓ Excellent tool stability



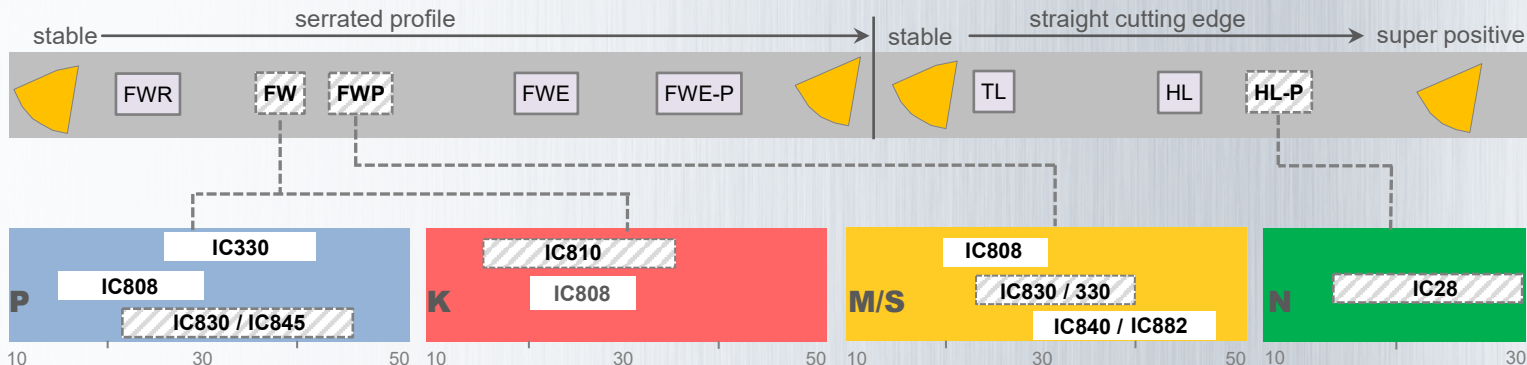
Product selection / chip formers / cutting grades

- End mills: Ø 20 – 40 mm *P290 EPW_*
- Shell mills: Ø 32 – 100 mm *P290 FPW_*
- Extended flute shell mill: Ø 32 – 100 mm *P290 SM / ACK_*
- Connections: shank / arbor / Flexfit
- Pitch: coarse, regular / each with internal coolant
- Insert sizes [mm]: 12 / 18
- Insert corner radii [mm]: special design, please refer to catalog
- Insert designs: ground = *P290 ACCT_* // pressed = *P290 ACKT_*

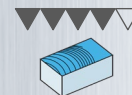
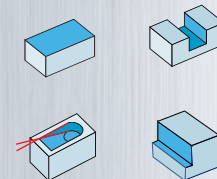


**Recommended
chip formers &
cutting grades**

For ISO-S / M / N materials
we recommend
ground insert options.



- ✓ Best productivity due to high feed per tooth
- ✓ Stable milling system
- ✓ First choice for series and mass production
- ✓ Wide selection of geometries
- ✓ Flexible use in ISO P / M / K / N / S materials



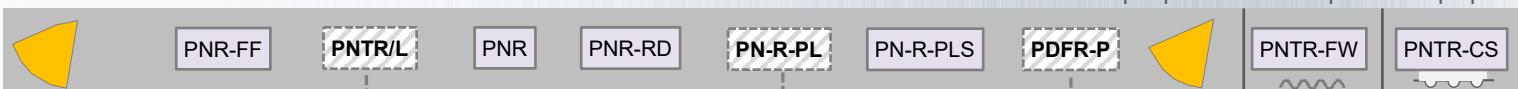
Product selection / chip formers / cutting grades

- End mills: Ø 16 – 50 mm [T490 ELN_](#)
- Shell mills: Ø 32 – 200 mm [T490 FLN_](#)
- Extended flute shell mill: Ø 32 – 80 mm [T490 LNK / SM_](#)
- Chamfering mill : Ø 50 – 125 mm [T422 / T445_](#)
- Connection: shank / arbor / MM / Flexfit
- Pitch: coarse, regular and fine pitch / each with internal coolant
- Insert sizes [mm]: 08 / 11 / 13 / 16 / 22
- Insert corner radii [mm]: 0.4 / 0.8 / 1.2 / 1.6 / 2.0 / 2.4 / 3.1 / 4.0 / 5.0 / 6.4
- Insert designs: ground = [T490 LNHT_](#) // pressed = [T490 LNMT_](#)

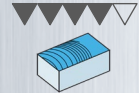
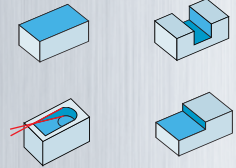
Recommended chip formers & cutting grades

For ISO-S / M / N we recommend ground insert options.

stable → super positive | shred profile | chip splitter



- ✓ 8 right-hand cutting edges
- ✓ Stable tool body
- ✓ Machining of 90° shoulders (no mismatch)
- ✓ Low power consumption
- ✓ Plus finishing inserts



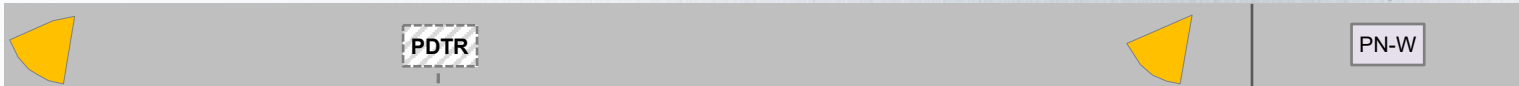
**Recommended
chip formers &
cutting grades**

Product selection / chip formers / cutting grades

- End mills: Ø 32 – 40 mm **T890 ELN_**
- Shell mills: Ø 40 – 160 mm **T890 FLN_**
- Connections: shank / arbor
- Pitch: coarse, regular and fine pitch / each with internal coolant
- Insert sizes [mm]: 13
- Insert corner radii [mm]: 0.8
- Insert designs: ground = **T890 LNH_(A)_T 1306_**



stable —————> super positive finishing insert



Feed per Tooth for HELIDO H690... 4 mm to 16 mm



ISO	Material		Condition	Tensile Strength [N/mm ²]	Hardness HB	Material No.	H690-04		H690-07			H690-10		H690-16	
							WNMU..._PNR-MM	WNMU..._PNTR	WNHU..._PNTR	WNMU..._PNTR	WNMU..._PNR-MM	TNCX..._PDR	TNCK..._PNTR	TNCK..._PNTR	
P	Non-alloy steel and cast steel, free cutting steel	< 0.25 %C	Annealed	420	125	1	0.10-0.11-0.15	0.10-0.11-0.15	0.1-0.15-0.2	0.15-0.2-0.35	0.15-0.20-0.35	0.10-0.11-0.13	0.10-0.12-0.15	0.15-0.22-0.30	
		>= 0.25 %C	Annealed	650	190	2									
		< 0.55 %C	Quenched and tempered	850	250	3									
		>= 0.55 %C	Annealed	750	220	4									
		>= 0.55 %C	Quenched and tempered	1000	300	5									
	Low alloy steel and cast steel (less than 5 % of alloying elements)			Annealed	600	200	6	0.08-0.12-0.14	0.08-0.11-0.14	0.08-0.14-0.18	0.15-0.20-0.33	0.15-0.20-0.33	0.07-0.09-0.11	0.08-0.10-0.14	0.15-0.20-0.28
				Quenched and tempered	930	275	7								
				Quenched and tempered	1000	300	8								
				Quenched and tempered	1200	350	9								
	High alloy steel, cast steel and tool steel			Annealed	680	200	10	0.08-0.09-0.12	0.08-0.09-0.12	0.08-0.12-0.16	0.15-0.18-0.28	0.15-0.18-0.28	0.07-0.08-0.10	0.08-0.10-0.12	0.15-0.18-0.24
Quenched and tempered				1100	325	11									
Stainless ferritic and stainless martensitic steel			Ferritic, martensitisch	680	200	12	0.08-0.10-0.13	0.08-0.10-0.13	0.08-0.12-0.17	0.15-0.18-0.31	0.15-0.18-0.31	0.07-0.09-0.11	0.08-0.10-0.13	0.15-0.18-0.26	
			Martensitic	820	240	13									
M	Stainless steel and stainless cast steel		Austenitic	600	180	14	0.08-0.10-0.13	-	0.08-0.12-0.17	-	0.09-0.15-0.25	0.06-0.08-0.11	0.08-0.10-0.13	0.09-0.16-0.21	
K	Grey cast iron (GG)		Ferritic/ martensitic	180	15	0.10-0.12-0.15	0.10-0.12-0.15	0.10-0.12-0.15	0.15-0.22-0.35	0.15-0.25-0.35	0.08-0.10-0.13	0.10-0.12-0.15	0.15-0.18-0.30		
			Pearlitic	260	16										
	Cast iron nodular (GGG)			Ferritic	160	17	0.08-0.11-0.14	0.08-0.11-0.14	0.08-0.11-0.14	0.15-0.20-0.33	0.15-0.20-0.33	0.07-0.09-0.11	0.08-0.11-0.14	0.15-0.18-0.26	
				Pearlitic	250	18									
Malleable cast iron			Ferritic	130	19	-	-	-	-	-	-	-	-		
			Pearlitic	230	20										
N	Aluminum wrought alloys			Not curable	60	21	-	-	-	-	-	-	-	-	
				Cured	100	22	-	-	-	-	-	-	-	-	-
	Aluminum cast alloys	<=12 % Si			Not curable	75	23	-	-	-	-	-	-	-	
					Cured	90	24	-	-	-	-	-	-	-	-
					Hyper-eutectic	130	25	-	-	-	-	-	-	-	-
	Copper alloys	>1 % Pb			Free cutting brass	110	26	-	-	-	-	-	-	-	
					Brass	90	27	-	-	-	-	-	-	-	-
					Electrolytic copper	100	28	-	-	-	-	-	-	-	-
	Non-ferrous				CFRP / GRP	29	29	-	-	-	-	-	-	-	
					Hard rubber	30	30	-	-	-	-	-	-	-	-
S	High temp. alloys	Fe Basis		Annealed	200	31	0.06-0.07-0.08	-	0.06-0.07-0.08	-	0.06-0.07-0.08	0.05-0.06-0.07	0.06-0.07-0.08	0.06-0.07-0.08	
				Cured	280	32									
				Annealed	250	33									
		Ni or Co Basis	Cured	350	34										
			Cast	320	35										
			Pure titanium	Rm = 400	Rm= 400	36									
	Titanium and Ti alloys		Alpha+beta alloy	Rm = 1050	Rm= 1050	37	0.08-0.09-0.10	-	0.08-0.09-0.10	-	0.08-0.09-0.10	0.06-0.07-0.08	0.08-0.10	0.08-0.10	
H	Hardened steel			Hardened	55 HRC	38	0.04-0.05-0.06	-	0.04-0.05-0.06	-	0.06-0.07-0.08	0.05-0.06-0.07	0.04-0.05-0.06	0.06-0.07-0.08	
				Hardened	60 HRC	39	-	-	-	-	-	-	-	-	
	Chilled cast iron		Cast	400	40	0.04-0.05-0.06	-	0.04-0.05-0.06	-	0.06-0.07-0.08	0.05-0.06-0.07	0.04-0.05-0.06	0.06-0.07-0.08		
	Cast iron		Hardened	55 HRC	41	0.04-0.05-0.06	-	0.04-0.05-0.06	-	0.06-0.07-0.08	0.05-0.06-0.07	0.04-0.05-0.06	0.06-0.07-0.08		

Feed per Tooth for HELIDO H490.. 9 mm to 17 mm



ISO	Material		Condition	Tensile Strength [N/mm ²]	Hardness HB	Material No.	H490 09 mm		H490 12 mm				H490 17mm			
							AN/CX PDR	AN/CX PNTR	AN/CX PDR	AN/CX PNTR	AN/CX PNTR-RM	AN/CX PNTR-CS	AN/CX PDR	AN/CX PNTR	AN/CX RM	AN/CX CS
P	Non-alloy steel and cast steel, free cutting steel	< 0.25 %C	Annealed	420	125	1	0.08-0.11-0.15	0.10-0.12-0.16	0.10-0.14-0.20	0.10-0.17-0.25	0.10-0.20-0.25	0.10-0.14-0.20	0.10-0.17-0.25	0.10-0.20-0.30	0.15-0.20-0.22	
			>= 0.25 %C	Annealed	650	190										2
		< 0.55 %C	Quenched and tempered	850	250	3										
			Annealed	750	220	4										
		>= 0.55 %C	Quenched and tempered	1000	300	5										
	Low alloy steel and cast steel (less than 5 % of alloying elements)	Annealed		600	200	6	0.08-0.10-0.15	0.08-0.10-0.16	0.08-0.10-0.20	0.08-0.10-0.20	0.08-0.12-0.20	0.10-0.12-0.20	0.08-0.10-0.20	0.08-0.10-0.25	0.08-0.10-0.25	0.15-0.16-0.22
				990	275	7										
		Quenched and tempered		1000	300	8										
				1200	350	9										
		High alloyed steel, cast steel and tool steel	Annealed	680	200	10										
Quenched and tempered	1100		325	11												
Stainless ferritic and stainless martensitic steel	Ferritic, martensitisch		680	200	12	0.08-0.10-0.14	0.08-0.10-0.16	0.08-0.10-0.18	0.08-0.12-0.20	0.08-0.12-0.20	0.08-0.10-0.18	0.08-0.10-0.18	0.08-0.10-0.20	0.08-0.10-0.20	0.12-0.16-0.20	
		Martensitic	820	240	13											
M	Stainless steel and stainless cast steel	Austenitic	600	180	14	0.08-0.10-0.14	0.08-0.10-0.16	0.08-0.10-0.20	0.08-0.10-0.20	-	0.08-0.10-0.20	0.08-0.10-0.20	0.08-0.10-0.20	-	-	
K	Grey cast iron (GG)	Ferritic/ martensitic		180	15	0.10-0.12-0.14	0.10-0.12-0.18	0.10-0.15-0.25	0.10-0.12-0.30	0.10-0.20-0.30	0.10-0.15-0.20	0.10-0.18-0.20	0.10-0.12-0.30	0.12-0.18-0.35	0.12-0.18-0.25	
				260	16											
	Cast iron nodular (GGG)	Ferritic		160	17	0.08-0.12-0.14	0.08-0.12-0.18	0.08-0.15-0.20	0.08-0.17-0.25	0.08-0.18-0.25	0.08-0.15-0.20	0.08-0.18-0.20	0.08-0.18-0.25	0.12-0.18-0.30	0.12-0.18-0.22	
			Pearlitic	250	18											
	Malleable cast iron	Ferritic		130	19	0.08-0.12-0.14	0.08-0.12-0.18	0.08-0.15-0.20	0.08-0.17-0.25	0.08-0.18-0.25	0.08-0.15-0.20	0.08-0.18-0.20	0.08-0.18-0.25	0.12-0.18-0.30	0.12-0.18-0.22	
Pearlitic			230	20												
N	Aluminum wrought alloys	Not curable		60	21	-	-	-	-	-	-	-	-	-	-	
			Cured	100	22											
	Aluminum cast alloys	Si <=12%	Not curable	75	23											
			Cured	90	24											
		>12% Si	Hyper-eutectic	130	25											
	Copper alloys	>1% Pb	Free cutting brass	110	26											
			Brass	90	27											
			Electrolytic copper	100	28											
	Non-ferrous	CFRP / GRP		29	29											
			Hard rubber	30	30											
S	High temp. alloys	Fe Basis	Annealed	200	31	-	-	-	-	-	-	-	-	-	-	
			Cured	280	32											
		Ni or Co Basis	Annealed	250	33											
			Cured	350	34											
			Cast	320	35											
	Titanium and Ti alloys	Pure titanium	Rm = 400	Rm= 400	36											
			Alpha+beta alloy	Rm = 1050	Rm= 1050											37
H	Hardened steel	Hardened		55 HRC	38	-	-	-	-	-	-	-	-	-	-	
				60 HRC	39											
	Chilled cast iron	Cast		400	40											
				55 HRC	41											

Feed per Tooth for HELITANG T490... 08 mm to 11 mm



ISO	Material		Condition	Tensile Strength [N/mm ²]	Hardness HB	Material No.	T490-08						T490-11				
							LNHT...PNR	LNMT...PNR	LNMT...CS	LNHT...RD	LNHT...PLS	LNAR...PNR-P	LNMT...PNTR	LNHT...PNTR	LNHT...PLS	LNMT...CS	LNMT...FW
P	Non-alloy steel and cast steel, free cutting steel	< 0.25 %C	Annealed	420	125	1	0.1-0.12-0.15	0.1-0.13-0.16	0.1-0.12-0.15	0.1-0.12-0.15	0.1-0.12-0.15	0.1-0.15-0.2	0.1-0.15-0.18	0.1-0.15-0.18	0.1-0.15-0.18	0.1-0.15-0.18	
			>= 0.25 %C	Annealed	650	190											2
		< 0.55 %C	Quenched and tempered	850	250	3											
			>= 0.55 %C	Annealed	750	220											4
		Low alloy steel and cast steel (less than 5 % of alloying elements)	Quenched and tempered	Annealed	1000	300											5
	Quenched and tempered			600	200	6											
	Quenched and tempered		930	275	7												
	Quenched and tempered		1000	300	8												
	High alloyed steel, cast steel and tool steel	Quenched and tempered	Annealed	680	200	10	0.08-0.10-0.12	0.08-0.11-0.12	0.08-0.10-0.12	0.08-0.10-0.12	0.08-0.10-0.12	0.1-0.12-0.14	0.1-0.12-0.14	0.1-0.12-0.14	0.1-0.12-0.14	0.1-0.12-0.14	
			Quenched and tempered	1100	325	11											
Stainless ferritic and stainless martensitic steel	Ferritic, martensitisch	Ferritic	680	200	12	0.08-0.10-0.13	0.08-0.10-0.13	0.08-0.10-0.13	0.08-0.10-0.13	0.08-0.10-0.13	0.1-0.14-0.18	0.1-0.12-0.14	0.1-0.12-0.14	0.1-0.12-0.14	0.1-0.12-0.14		
		Martensitic	820	240	13												
M	Stainless steel and stainless cast steel	Austenitic	600	180	14	0.08-0.10-0.13	0.08-0.10-0.13	0.08-0.10-0.13	0.08-0.10-0.13	0.08-0.10-0.13	0.1-0.13-0.16	0.08-0.12-0.14	0.08-0.12-0.14	0.08-0.12-0.15	0.08-0.12-0.15		
K	Grey cast iron (GG)	Ferritic, martensitic	Ferritic	180	15	0.1-0.12-0.15	0.1-0.13-0.15	0.1-0.12-0.15	0.1-0.12-0.15	0.1-0.12-0.15	0.1-0.15-0.25	0.1-0.15-0.2	0.1-0.15-0.2	0.1-0.15-0.2	0.1-0.15-0.2		
			Pearlitic	260	16												
	Cast iron nodular (GGG)	Ferritic	Ferritic	160	17	0.08-0.12-0.14	0.08-0.13-0.14	0.08-0.12-0.14	0.08-0.12-0.14	0.08-0.12-0.14		0.1-0.14-0.18	0.1-0.14-0.18	0.1-0.14-0.18	0.1-0.14-0.18		
			Pearlitic	250	18												
	Malleable cast iron	Ferritic	Ferritic	130	19												
Pearlitic			230	20													
N	Aluminum wrought alloys	Not curable	Aluminum	60	21	0.1-0.15-0.20	-	-	-	-	-	-	-	-	-		
			Cured	100	22												
	Aluminum cast alloys	<=12% Si	Not curable	Aluminum	75											23	
				Cured	90											24	
	>12% Si	Hyper-eutectic	130	25													
		Free cutting brass	110	26													
	Copper alloys	>1% Pb	Brass	90	27												
			Electrolytic copper	100	28												
	Non-ferrous	CFRP / GRP	CFRP / GRP	29	29												
			Hard rubber	30	30												
S	High temp. alloys	Fe Basis	Annealed	200	31	0.06-0.07-0.08	-	0.06-0.07-0.08	0.06-0.07-0.08	0.06-0.07-0.08	0.06-0.07-0.08	0.05-0.07-0.08	0.05-0.07-0.08	0.05-0.07-0.08	0.05-0.07-0.08		
			Cured	280	32												
		Ni or Co Basis	Annealed	250	33												
			Cured	350	34												
		Cast	320	35													
	Titanium and Ti alloys	Pure titanium	Rm = 400	Rm = 400	36	0.08-0.09-0.1	-	0.08-0.09-0.1	0.08-0.09-0.1	0.08-0.09-0.1	0.08-0.09-0.1	0.06-0.08-0.1	0.06-0.08-0.1	0.06-0.08-0.1	0.06-0.08-0.1		
			Alpha+beta alloy	Rm = 1050	Rm = 1050											37	
	H	Hardened steel	Hardened	55 HRC	38	-	-	-	-	-	-	0.05-0.06-0.08	-	-	-		
60 HRC				39	-	-	-	-	-	-	-	-	-				
Chilled cast iron		Cast	400	40	-	-	-	-	-	-	0.05-0.06-0.08	-	-	-			
			55 HRC	41	-	-	-	-	-	-	0.05-0.06-0.08	-	-	-			

Feed per Tooth for HELIDO S890... 13 & NEODO S890... 08



ISO	Material		Condition	Tensile Strength [N/mm ²]	Hardness HB	Material No.	V _c [m/min]	S890-13			S890-08				
								SNMU PNTR	SNMU MM	SNMU PNTN	SZMU PNR MM	SZMU PNTR	SZMU PNRHP	SZHU PNR	
P	Non-alloy steel and cast steel, free cutting steel		< 0.25 %C	Annealed	420	125	1	140-180-250	0.10-0.15-0.25	0.10-0.15-0.30	0.10-0.15-0.25	0.10-0.15-0.25			
			>= 0.25 %C	Annealed	650	190	2								
			>= 0.55 %C	Quenched and tempered	850	250	3								
			>= 0.55 %C	Annealed	750	220	4								
			>= 0.55 %C	Quenched and tempered	1000	300	5								
	Low alloy steel and cast steel (less than 5 % of alloying elements)			Annealed	600	200	6	130-160-200	0.08-0.15-0.20	0.08-0.10-0.20	0.08-0.10-0.20	0.1-0.12-0.20			
					930	275	7								
					1000	300	8								
				Quenched and tempered	1200	350	9								
	High alloyed steel, cast steel and tool steel			Annealed	680	200	10	120-130-180	0.08-0.14-0.18	0.08-0.14-0.18	0.08-0.14-0.18	0.08-0.10-0.15			
Quenched and tempered				1100	325	11									
Stainless ferritic and stainless martensitic steel			Ferritic, martensitisch	680	200	12	90-110-160	0.08-0.12-0.20	0.08-0.12-0.20	0.08-0.12-0.20	0.08-0.10-0.15		0.08-0.10-0.20		
			Martensitic	820	240	13									
M	Stainless steel and stainless cast steel		Austenitic	600	180	14	80-140-180	0.08-0.10-0.20	0.08-0.10-0.20	0.08-0.10-0.20	0.08-0.10-0.15		0.08-0.12-0.20	0.08-0.10-0.20	
K	Grey cast iron (GG)		Ferritic/ martensitic	180	15	140-180-280	0.10-0.12-0.30	0.10-0.12-0.35	0.10-0.12-0.30		0.10-0.15-0.25				
			Pearlitic	260	16										
	Cast iron nodular (GGG)			Ferritic	160	17	120-160-250	0.08-0.16-0.25	0.08-0.18-0.25	0.08-0.18-0.25		0.10-0.15-0.20			
				Pearlitic	250	18									
	Malleable cast iron			Ferritic	130	19									
Pearlitic				230	20										
N	Aluminum wrought alloys			Not curable	60	21									
				Cured	100	22									
				Not curable	75	23									
	Aluminum cast alloys	<=12% Si			Cured	90	24								
					Hyper-eutectic	130	25								
	Copper alloys	>12% Si	>1% Pb		Free cutting brass	110	26								
					Brass	90	27								
					Electrolytic copper	100	28								
					CFRP / GRP		29								
					Hard rubber		30								
S	High temp. alloys	Fe Basis		Annealed	200	31	20-60-100								
				Cured	280	32									
		Ni or Co Basis			Annealed	250	33	20-35-80							
					Cured	350	34								
	Titanium and Ti alloys				Cast	320	35								
					Pure titanium	Rm = 400	Rm= 400							36	
					Alpha+beta alloy	Rm = 1050	Rm= 1050							37	
H	Hardened steel			Hardened	50 HRC	38	40-60-120	-	-	-	0.06-0.08-0.12	-	-		
				Hardened	60 HRC	39	-	-	-	-	-				
	Chilled cast iron				Cast	400	40	-	-	-	-	-			
					Cast iron	Hardened	55 HRC	41	-	-	-	-			



Feed per Tooth for LOGIQ8Tang T890... 13 mm

ISO	Material	Hardness HB	Material No.	V _c [m/min]	T890-13		
					LNHT... PNTR	LNAT... PN-W	
P	Non-alloy steel and cast steel, free cutting steel	< 0.25 %C	125	1	140-180-250	0.12-0.16-0.2	0.12-0.16-0.2
		>= 0.25 %C	190	2			
		< 0.55 %C	250	3			
		>= 0.55 %C	220	4			
			300	5			
	Low alloy steel and cast steel (less than 5 % of alloying elements)		200	6	130-160-200	0.1-0.14-0.18	0.1-0.14-0.18
			275	7			
			300	8			
	High alloyed steel, cast steel and tool steel		350	9	130-140-180	0.1-0.13-0.15	0.1-0.12-0.15
			200	10	120-130-180	0.1-0.12-13	0.1-0.11-0.13
		325	11				
	Stainless ferritic and stainless martensitic steel		200	12	90-110-160	0.1-0.12-0.15	0.1-0.12-0.15
		240	13				
M	Stainless steel and stainless cast steel	180	14	80-140-180	-	-	
K	Grey cast iron (GG)	180	15	140-180-280	0.1-0.15-0.2	0.1-0.15-0.2	
		260	16				
	Cast iron nodular (GGG)	160	17	120-160-250	0.1-0.14-0.18	0.1-0.14-0.18	
		250	18				
	Malleable cast iron	130	19				
		230	20				

Radius for programming

System	T490 LNHT 1306-FF	H490 ANKX 0904-FF	H490 ANKX 1205-FF	H490 ANKX 1706-FF
Radius for programming	1,95	1,2	2,5	2,85

Screw & Torque

System	HM390 TP.. 04	HM390 TP.. 05	HM390 TC.. 07	HM390 TC.. 10	HM390 TD.. 15	HM390 TD.. 19	T490 LN.. 08	T490 LN.. 11	T490 LN.. 13	T490 LN.. 16	T490 LN.. 22
Screw	SR M2X0.4-3.5 T6	TS 180411/HG	SR M2.5X5-T7-60	SR 14-562/S	SR 10511869	SR 14-591/L12	SR 10502813-HGSM	SR 34-535-SN	SR 34-535-SN	SR 14-591	SR 10507547
Torque	0.5 N/m	0.5 N/m	0.9 N/m	3.2 N/m	9 N/m	9 N/m	1.2 N/m	3.2 N/m	4.8 N/m	9 N/m	9 N/m
H690 WN.. 04	H690 WN.. 07	H690 TN.. 10	H690 TN.. 16	H490 AN.. 09	H490 AN.. 12	H490 AN.. 17	S890 SZ.. 08	S890 SN.. 13	P290 AC.. 12	P290 AC.. 18	T890 LN.. 13
SR M2.5X6-T7-60 0.9 N/m	SR M4X0.7IP15 4.8 N/m	SR 10508082-HG 1.2 N/m	SR 14-591 9 N/m	SR 10508082-HG 1.2 N/m	SR 14-544 4.8 N/m	SR 14-591 9 N/m	SR M3X0.5-L7.4 IP9 2 N/m	SR 11800745 4.8 N/m	SR M3X0.5-L7.4 IP9 2 N/m	SR 14-544/S 4.8 N/m	SR 10513105 8 N/m

Helical interpolation in full material

MDN - MDX & RPMX°																							
Tool body diameter	Ø 6	Ø 8	Ø 10	Ø 12	Ø 14	Ø 16	Ø 18	Ø 20	Ø 22	Ø 25	Ø 28	Ø 32	Ø 40	Ø 50	Ø 63	Ø 80	Ø 100	Ø 125	Ø 160	Ø 200	Ø 250	Ø 315	
HM390 TPKR 0401		13.4 - 15 3°	17.4 - 19 2.5°																				
HM390 TPKT 0502	8 - 11 1°	12 - 15 1°	16 - 19 2°	20 - 23 1.5°	24 - 27 1.5°	28 - 31 1.5°		35.6 - 39 2.0°		45.6 - 49 1.5°													
HM390 TCKT 0703					25 - 27 1.9°	29 - 31 1.9°	33 - 35 1.4°	37 - 39 1.4°	41 - 43 1°	47 - 49 1°	53 - 55 1°	61 - 63 0.8°	77 - 79 0.6°										
HM390 TCKT 1003										46.4 - 49 2.9°	52.4 - 55 2.5°	60.4 - 63 2.1°	76.4 - 79 1.6°	96.4 - 99 1.2°	122.4 - 125 0.9°								
HM390 TDKT 1505													75 - 78.4 2.1°	93 - 98.4 1.5°	121 - 124.4 1.20°	155 - 158.4 0.90°	195 - 198.4 0.70°	245 - 248.4 0.50°	315 - 318.4 0.30°	395 - 398.4 0.20°			
HM390 TDKT 1907													73 - 78.4 2°	93 - 98.4 1.5°	119 - 124.4 1.10°	153 - 158.4 0.90°	193 - 198.4 0.70°	243 - 248.4 0.50°	313 - 318.4 0.40°				
H690 WNMU 0403						28 - 35.2 1.7°	32 - 39.2 1.5°		42 - 49.2 1.1°			56 - 63.2 0.8°	72 - 79.2 0.6°	92 - 99.2 0.5°	118 - 125.2 0.2°								
H690 WNMU 0703												54 - 62.4 2°	70 - 78.4 1.5°	90 - 98.4 1.2°	116 - 124.4 1.1°	150 - 158.4 1°	190 - 198.4 0.8°	240 - 248.4 0.5°					
H690 TNKX 1005							34.8 - 39.2 2.8°		44.8 - 49.2 2.6°			58.8 - 63.2 1.6°	74.8 - 79.2 1.1°	94.8 - 99.2 1°	120.8 - 125.2 0.7°								
H690 TNKX 1606														88.4 - 98 3°	114.4 - 124 2°	148.4 - 158 1°	188.4 - 198 1°	238.4 - 248 0.5°					
P290 ACCT 1204							25 - 38.2 2°		35 - 48.2 1.4°			49 - 62.2 1°	65 - 78.2 0.7°	85 - 98.2 0.5°									
P290 ACCT 1806									32.8 - 47.6 2.5°			46.8 - 61.6 2°	62.8 - 77.6 1.5°	82.8 - 97.6 1°	108.8 - 123.6 0.8°	142.8 - 157.6 0.5°	182.8 - 197.6 0.3°						
T490 LNMT 0804-RD					24.4 - 31.2 2.8°	28.4 - 35.2 2.3°	32.4 - 39.2 1.9°	36.4 - 43.2 1.6°	42.4 - 49.2 1.3°			56.4 - 63.2 0.9°	72.4 - 79.2 0.7°	92.4 - 99.2 0.5°									
T490 LNHT 1306-RD												52.8 - 62.4 2.8°	68.8 - 78.4 2°	88.8 - 98.4 1.5°	114.8 - 124.4 1.1°	148.8 - 158.4 0.9°	188.8 - 198.4 0.7°	238.8 - 248.4 0.5°					
T490 LNHT 1306-FF												53.6 - 62.4 3.9°	69.6 - 78.4 2.8°	89.6 - 98.4 2°	115.6 - 124.4 1.5°	149.6 - 158.4 1.1°	189.6 - 198.4 0.9°	239.6 - 248.4 0.7°	309.6 - 318.4 0.5°	389.6 - 398.4 0.4°	489.6 - 498.4 0.3°		
H490 ANKX 0904-FF					22.4 - 30 7.7°	26.4 - 34 5.7°	30.4 - 38 4.6°	34.4 - 42 3.8°	40.4 - 48 3°			54.4 - 62 2°	70.4 - 78 1.5°	90.4 - 98 1.1°	116.4 - 124 0.8°								
H490 ANKX 1205-FF									33.8 - 47 6.1°			47.8 - 61 3.3°	63.8 - 77 2.2°	83.8 - 97 1.5°	109.8 - 123 1.1°	143.8 - 157 0.8°	183.8 - 197 0.6°	233.8 - 247 0.4°	303.8 - 317 0.3°	383.8 - 397 0.2°			
H490 ANKX 1706-FF												46.6 - 60.8 6.5°	62.6 - 76.8 4°	82.6 - 96.8 2.7°	108.6 - 122.8 1.9°	142.6 - 156.8 1.4°	182.6 - 196.8 1°	232.6 - 246.8 0.8°	302.6 - 316.8 0.6°	382.6 - 396.8 0.4°	482.6 - 496.8 0.3°	612.6 - 626.8 0.2°	

MDN – MDX = Minimum – maximum diameter in mm for Helical interpolation in full material

RPMX° = Maximum ramp angle

Rg = Radius for programming

If a pilot hole is made, the minimum diameter (MDN) can also be selected smaller.

Formula for the pre-drilling: $D_{min} (MDN) = D_{set} + 1$

Recommended Cutting Speeds and Applications According to Cutting Grades

Based on practical experience – average data

Grades with PVD coatings and Cermet

Material Group	IC330			IC380			IC845			IC840			IC830			IC716			IC882			IC810			IC808			IC30N						
	min.	to start	max.	min.	to start	max.	min.	to start	max.	min.	to start	max.	min.	to start	max.	min.	to start	max.	min.	to start	max.	min.	to start	max.	min.	to start	max.	min.	to start	max.				
P Non-alloy / alloy steel	1. Choice	—			—			—			—			—			—			—			—			—			—			—		
	2. Choice	120	160	230	160	200	250	80	150	220	---	---	120	200	230	---	---	---	160	220	250	180	230	250	90	220	350	---	---	---	---			
P Ferritic / martensitic steel	1. Choice	—			—			—			—			—			—			—			—			—			—			—		
	2. Choice	80	120	140	---	---	---	100	120	160	---	---	100	130	160	---	---	---	---	---	---	140	170	220	100	170	220	---	---	---	---			
M Stainless steel Reference: 1.4301, v,200, try 1.4404, v,90, wet 1.4462, v,80, wet	1. Choice	—			—			—			—			—			—			—			—			—			—			—		
	2. Choice	60	100	160	120	160	220	---	---	---	90	120	160	60	140	200	---	---	70	100	140	---	---	---	120	160	220	---	---	---	---			
K Gray cast iron	1. Choice	---			---			---			---			---			---			---			---			---			---			---		
	2. Choice	---	---	---	---	---	---	---	---	---	---	---	120	160	250	---	---	---	---	---	180	250	300	---	---	---	---	---	---	---	---			
K Cast iron nodular	1. Choice	---			---			---			---			---			---			---			---			---			---			---		
	2. Choice	---	---	---	---	---	---	---	---	---	---	---	120	140	200	---	---	---	---	---	160	200	260	160	180	250	---	---	---	---	---			
S High temp / titan alloys	1. Choice	—			—			---			—			—			—			—			---			—			---			---		
	2. Choice	30	40	100	30	50	100	---	---	---	25	40	90	30	40	100	20	45	70	20	40	60	---	---	---	30	50	100	---	---	---	---		
N Aluminum / non ferrous	1. Choice	---			---			---			---			---			---			---			---			---			---			---		
	2. Choice	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---		
H Hardened steel (≤55Hrc)	1. Choice	---			---			---			---			---			---			---			---			---			---			---		
	2. Choice	---	---	---	---	---	---	---	---	---	---	---	40	80	120	---	---	---	---	---	60	100	150	80	120	200	50	100	140	---	---			

Legend: Cutting speed declaration (m/min)
 red line: — dry machining
 blue line: — wet machining
 bold font: — recommended start value

Recommended Cutting Speeds and Applications According to Cutting Grades


Based on practical experience – average data


Grades with CVD coatings, Ceramics, CBN and uncoated

Material Group	IC5400			IC5500			IC5600			IC5100			DT7150			IC5820			IS8/IS80			IB55/IB85			IC28			IC08		
	min.	to start	max.	min.	to start	max.	min.	to start	max.	min.	to start	max.	min.	to start	max.	min.	to start	max.	min.	to start	max.	min.	to start	max.	min.	to start	max.			
P Non-alloy / alloy steel	1. Choice																---			---			---			---				
	2. Choice				---			---			---			---			---			---			---			---				
P Ferritic / martensitic steel	1. Choice										---			---			---			---			---			---				
	2. Choice				---			---			---			---			---			---			---			---				
M Stainless steel	1. Choice				---			---			---			---						---			---			---				
	2. Choice				---			---			---			---			---			---			---			---				
K Gray cast iron	1. Choice	---			---			---									---						Please ask your Product Management			---				
	2. Choice	---			---			---			---			---			---			---			---			---				
K Cast iron nodular	1. Choice				---			---			---						---						---			---				
	2. Choice				---			---			---			---			---			---			---			---				
S High temp / titan alloys	1. Choice	---			---			---			---			---						---			---							
	2. Choice	---			---			---			---			---			---			---			---			---				
N Aluminum / non ferrous	1. Choice	---			---			---			---			---			---			---										
	2. Choice	---			---			---			---			---			---			---			---			---				
H Hardened steel (≤55HRC)	1. Choice	---			---			---			---			---			---			---			Please ask your Product Management			---				
	2. Choice	---			---			---			---			---			---			---			---			---				

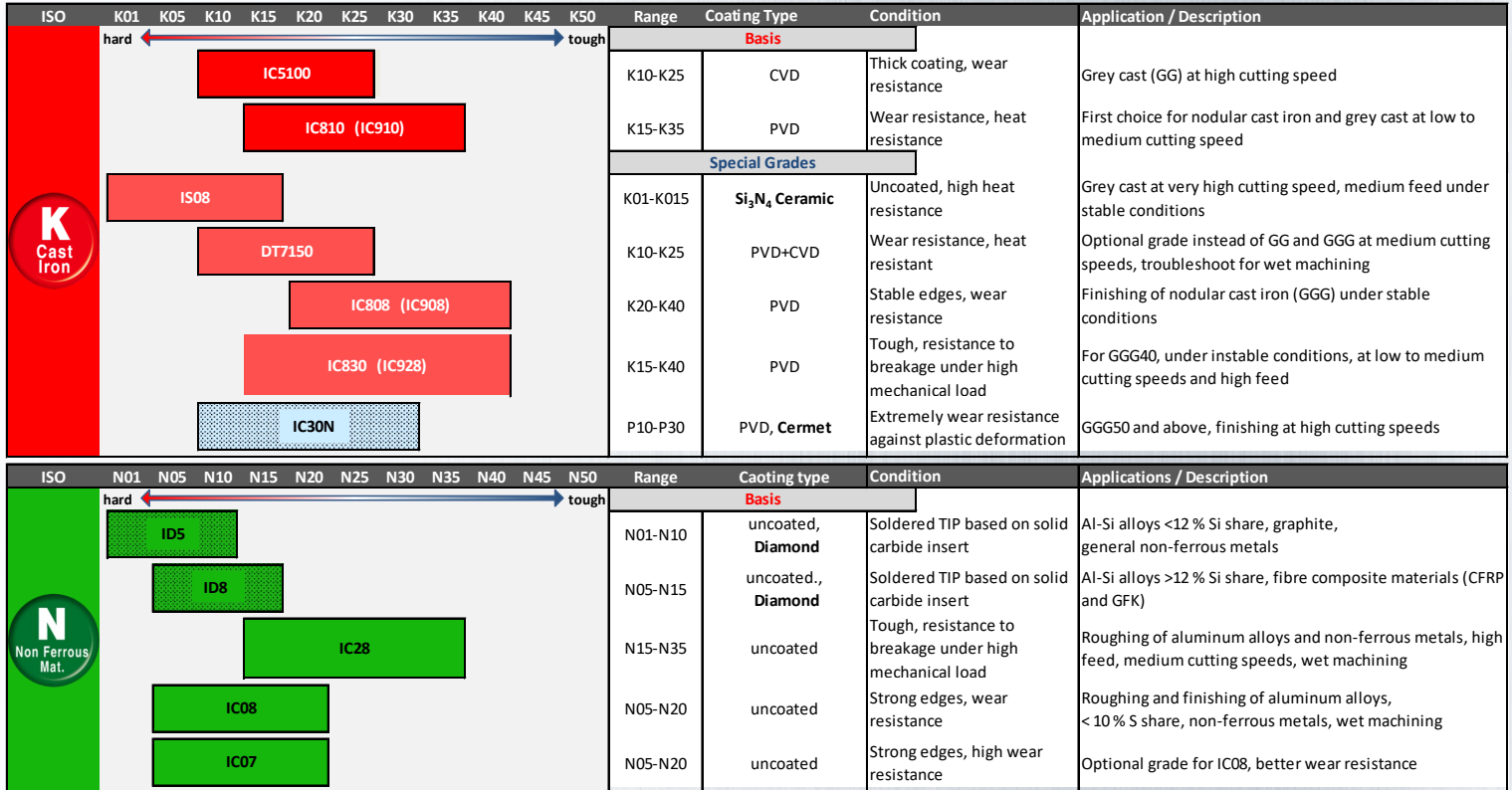
Legend: Cutting speed declaration (m/min)
 red line: dry machining
 blue line: wet machining
 bold font: recommended start value

Milling Inserts – Cutting Grades


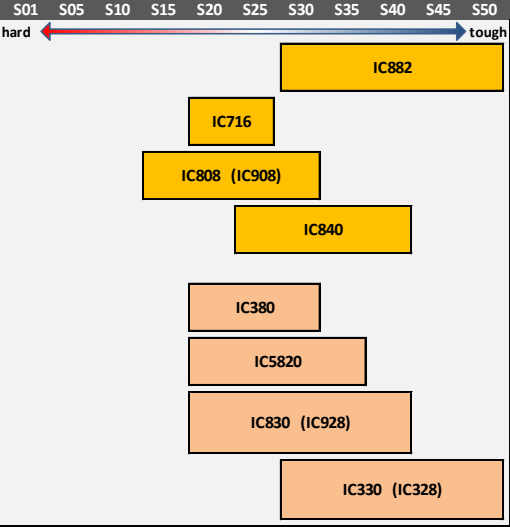

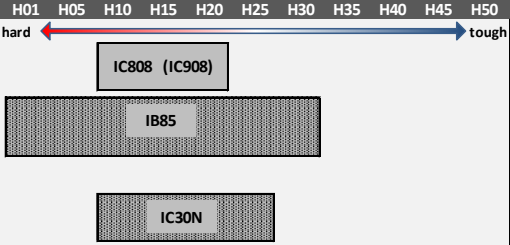
ISO	P01	P05	P10	P15	P20	P25	P30	P35	P40	P45	P50	Range	Coating Type	Condition	Applications / Description
												Basis			
					IC808 (IC908)							P15-P30	PVD	Strong edge, wear resistance	Roughing, Roughing under stable conditions, medium to high cutting parameters
				IC5600								P10-P15	CVD	Stable heat, strong edge, high wear resistance	Roughing and finishing under stable conditions, high cutting speed, dry machining
					IC5500							P15-P35	CVD	Stable heat, wear resistance	Roughing, ferritic and martensitic high alloyed steel (group 12 and 13), high cutting speed, dry machining
					IC830 (IC928)							P20-P40	PVD	Tough, no breakage under mechanical load	Universal cutting grade, basic grade for initial machining, roughing, wet or dry
						IC845						P30-P50	PVD	Tough, no breakage, thermal crack resistance	Roughing at high feed, interrupted cut
				IC5400									Special Grades		
					IC30N							P05-P20	CVD	Stable heat resistance, wear resistance	Roughing at medium to high cutting speed, dry machining
					IC810 (IC910)							P10-P30	PVD, Cermet	Strong wear resistance against plastic deformation	Finishing at high cutting speeds and medium feed
						IC810 (IC910)						P15-P30	PVD	Wear resistance, stable to breakage	Roughing of high-strength steel and tool steel (group 10 and 11), at medium feed
						IC330 (IC328)						P25-P50	PVD, TiCN	Tough, no breakage, thermal crack resistance	Roughing at low cutting speed, interrupted cut, wet machining only

ISO	M01	M05	M10	M15	M20	M25	M30	M35	M40	M45	M50	Range	Coating Type	Condition	Applications / Description	
												Basis				
					IC840							M20-M40	PVD	Tough, thermal crack resistance	Roughing and finishing at low to medium cutting speed, wet or dry machining	
					IC830 (IC928)							M25-M35	PVD	Tough, resistance to breakage under high mechanical load	Universal grade for austenitic steel, low to medium cutting speed, wet or dry machining	
					IC808 (IC908)							M20-M30	PVD	Strong edges, wear resistance	Finishing at medium to high cutting speed under stable conditions, wet or dry machining	
						IC330 (IC328)						M30-M40	PVD	Tough, resistance to breakage under high mechanical load	Universal grade for austenitic steel, low cutting speed, interrupted cut, wet machining only	
					IC5820								M20-M35	CVD	Tough, resistance to breakage, heat resistance	Roughing in austenitic and Duplex materials at high cutting speed under stable conditions
						IC882							M25-M45	PVD	Tough, resistance to breakage, heat resistance	Roughing in austenitic and Duplex materials at low to medium cutting speed, wet machining
												Special Grades				

Milling Inserts – Cutting Grades



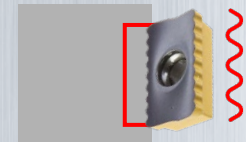
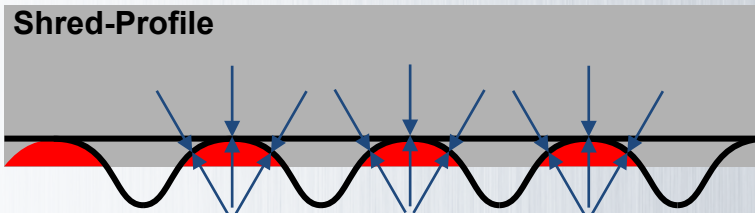
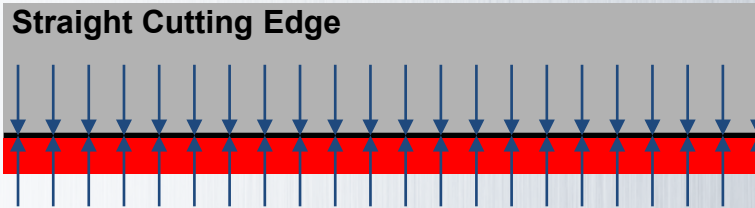
Milling Inserts – Cutting Grades

ISO	S01	S05	S10	S15	S20	S25	S30	S35	S40	S45	S50	Range	Coating Type	Condition	Applications / Description
												Basis			
	S30-S50		PVD	Tough, h. heat resistance, contains Rutenium	Roughing and finishing of HTSA, low to medium cutting speeds, wet machining only										
	S20-25		PVD	Tough, h. heat resistance, thermal crack resistance	Roughing and finishing of titanium alloys (ISO S36-S37) at medium cutting speeds.										
	S15-S30		PVD	Strong edges, wear resistance	Finishing under stable conditions, medium cutting speed										
	S25-S40		PVD	Tough, thermal crack resistance	Roughing of Ti-alloys, low cutting speed, wet machining only										
	Special Grades														
	S20-S30		PVD	Strong edges, wear resistant, special cutting	Roughing and finishing of titanium under lable conditions, wet machining only										
S20-S35		CVD	High heat resistance, wear resistance, +Rutenium	Optional grade for IC882, high cutting speed, wet and dry machining											
S20-S40		PVD	Tough, resistance to breakage under high mechanical load	Optional grade for IC840 and IC808 at low cutting speeds, high feed, wet machining.											
S30-S50		PVD	Tough, resistance to breakage under high mechanical load	Optional grade for IC840, IC808, IC830, high thermal crack resistance, sufficient coolant supply is essential											
ISO	H01	H05	H10	H15	H20	H25	H30	H35	H40	H45	H50	Range	Coating Type	Condition	Applications / Description
												Basis			
	H10-H20		PVD	Strong edges, resistance to breakage	Hardened steel up to 55 HRC (max. 60 HRC), under stable conditions, down-mill only, max. 45 % a _p /D										
	H01-H30		no coating, CBN	Soldered TIP based on solid carbide insert, resistance to breakage	Finishing of hardened steel up to 65 HRC, up-mill if possible										
Special Grades															
H10-H25		PVD, Cermet		Finishing under stable conditions at high cutting speeds											

Contact length determines cutting force!

Effects of reduced contact area due to shred profile:

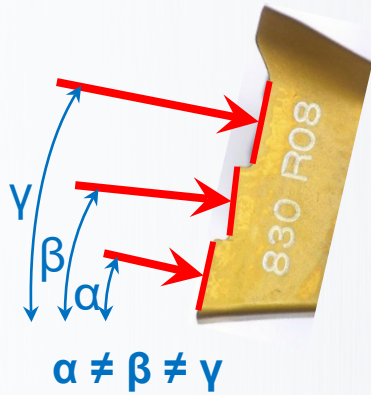
- 20 – 30% less cutting forces
- lower temperature development
- less repulsive forces
- reduced noise development



Indexable inserts with **...-FW** in the designation

Unique geometry for segmenting the chips

Distribution of forces



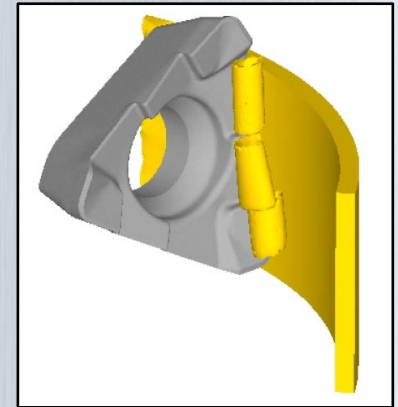
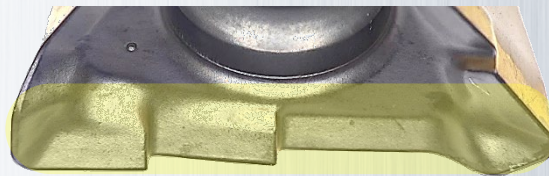
Chips segmentation



Effects through HELISTAR - Geometry:

- 10 – 15% less cutting forces
- less repulsive forces
- reduced noise development

Highly positive, soft-cutting geometry



Indexable inserts with **...-HS** in the designation

Correction factors depending on the cantilever length/stability factor

Counteracting by reducing the cutting data

Correction factor for various tool length

Overhang ratio	up to 1 x D	up to 2 x D	up to 3 x D	up to 4 x D	up to 5 x D
Factor f_z	1,00	0,95	0,85	0,75	0,65
Factor v_c	1,00	1,00	0,80	0,70	0,60

Example:

$$L/D = 150/50 = 3$$

Feed correction factor

Tooth feed selected: 0.26 mm

Cutting speed selected: 180 m/min

Alternatively, you can also use the stability factor k_s !

The factor is determined by the following: Assessment of the milling process determines:

$k_s = 1.0$ • With regular stability

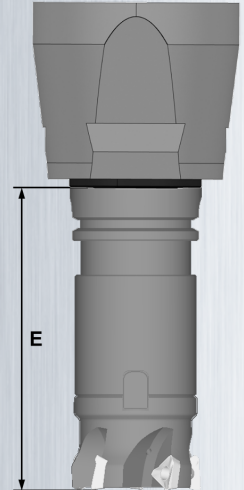
$k_s = 0.7$ • For unstable machining (large projection length, unstable clamping, thin-walled workpieces, etc.)

Example:

Stability factor k_s 0.7 selected

To be used f_z : $0,26 \times 0,7 = 0,182$ mm

To be used v_c : $180 \times 0,7 = 126$ m/min



Not valid when using high feed milling cutters

Bending Moment Load

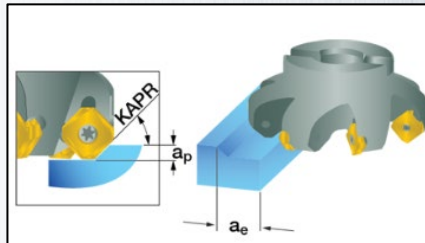
The longer the tool overhang, the more important it is to consider the bending moment. Too high a bending moment can lead to massive spindle damage.

The bending moment can be calculated using the formula or using machining power. The load limits can be requested from the machine manufacturer.

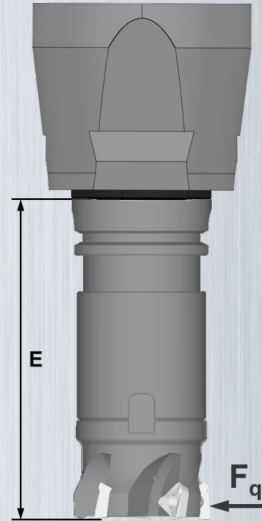
Calculate the spindle bending moment using the Machining Power tool : <https://mpwr.iscar.com>

MP²

Machining Power (Full)
Vc/n - Cutting / Spindle speed
Vf - Feed speed
P/T - Power / Torque
Q - Material removal rate
F - Cutting forces
h - Chip thickness
T - Cutting time
a _e - Max. cutting width
M - Max. spindle bending moment



Cutting diameter (DC):	<input type="text" value="63"/>	mm
Cutting width (a _e):	<input type="text" value="42"/>	mm
Face effective cutting edge count (ZEPF):	<input type="text" value="5"/>	
Feed per tooth (f _z):	<input type="text" value="0.2"/>	mm
Depth of cut (a _p):	<input type="text" value="4"/>	mm
Workpiece material:	<input type="text" value="C45E; Ck 45"/>	DIN
Tool cutting edge angle (KAPR):	<input type="text" value="90"/>	deg.
Effective rake angle (γ):	<input type="text" value="5"/>	deg.
Tool extension (E):	<input type="text" value="250"/>	mm
<input type="button" value="Reset"/> <input type="button" value="Calculate"/>		
Max spindle bending force:	2.818,88	N
Max spindle bending moment:	704,72	Nm



$$M_b = F_q \times E \text{ [Nm]}$$

General Guide Values

Interfaces	Bending moment limit [Nm]
HSK32	85
HSK40	140
HSK50	230
HSK63	450
HSK80	810
HSK100	1230
HSK125	2900
Big Plus 40	45
Big Plus 50	60
C5	420
C6	700
C8	1000
C10	1700
Driven tool holders	
VDI30	80
VDI40	150

We cannot take a guarantee for the specified guideline values.

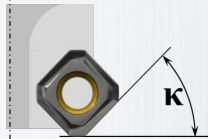
Recommended chip thickness h guidelines

General recommendations (for stable conditions)

ISO	Material	Roughing	Medium Application	Finishing
P	Steel	0,12 - 0,22 mm	0,10 - 0,16 mm	0,04 - 0,08 mm
M	Stainless Ssteel	0,12 - 0,18 mm	0,08 - 0,14 mm	0,04 - 0,08 mm
K	Cast Iron	0,12 - 0,25 mm	0,10 - 0,20 mm	0,04 - 0,08 mm
S	Highly Heat Resistant M.	0,08 - 0,10 mm	0,06 - 0,08 mm	0,04 - 0,08 mm

Kappa:	Sinus-value:
90°	1
60°	0,87
45°	0,71
30°	0,5

$$f_z = \frac{h}{\sin \kappa}$$



Valid for $a_e/D > 33\%$

The attack angle Kappa must be taken into account.

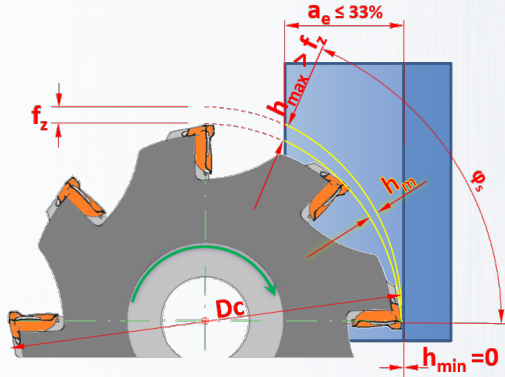
Not valid when using high feed milling cutters

Calculate recommended feed per tooth f_z with cutting width $\leq 33\%$

When milling with a cutting width of $\leq 33\%$, the maximum chip thickness h_{max} is always significantly smaller than f_z .

Under these conditions we recommend calculating the feed using the center chip thickness h_m .

Calculating the correct f_z with formula:



Formula f_z :

Feed per tooth

$$f_z = h_m \times \sqrt{Dc/ae} \quad [\text{mm}]$$

Example:

With a cutting width (a_e 18 mm / Dc 63 mm) of 29%, a tooth per feed of 0.17 mm should be used in order to achieve the necessary center chip thickness and the associated process reliability and cost-effectiveness.

Step 1:

Select recommended f_z from tooth feed table.

S890-13
SNMU MM
0.10-0.15-0.30

Step 2:

Middle chip thickness h_m calculation by using factor of 0.6

$$h_m = \underline{0,6} \times \text{recommended } f_z \text{ value}$$

Step 3:

Feed per tooth f_z calculation

Feed per tooth

$$f_z = h_m \times \sqrt{Dc/ae} \quad [\text{mm}]$$

Example calculation:

$$h_m = 0,15 \cdot 0,6 = \underline{0,09 \text{ mm}}$$

$$f_z = 0,09 \cdot \sqrt{(63 / 18)} = \underline{0,17 \text{ mm}}$$

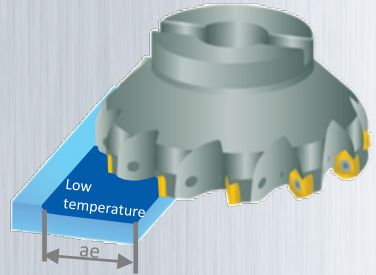
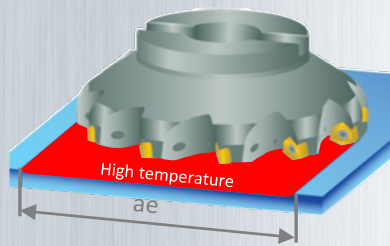
Cutting Speed Adjustment

Increased productivity by cutting speed adjustment [m/min] depending on actual width of cut

The real temperature volume depends on the basic cutting speed value and the width of cut in relation to the cutter diameter (E%). Usually, the cutting speed is adjusted after the first tool life(s) determined. The reason why is that the real temperature in the cutting zone is normally not measured.

Basic rules:

1. If most of the temperature is conducted via the chips, it is possible to increase the cutting speed.
2. The better the overall stability (short overhang, no vibrations), the better the options to adjust the cutting speed.
3. The lower the specific thermal conductivity, the less options for cutting speed adjustments. With the help of the below thermal conductivity table of various material groups you may better judge the options for cutting speed adjustments. There are exceptions in the field of special alloys.
4. Main wear should be flank wear.



$E\% = a_e / D_c \cdot 100 (\%)$	5%	10%	15%	20%	25%	30%
Factor for v_c	1,50	1,45	1,40	1,35	1,30	1,25

↓

$$v_c = v_o \cdot Factor$$

Thermal conductivity: [W/(mK)]

↓	Al alloys:	+/- 150
↓	Carbon steel:	+/- 50
↓	Tool steel:	+/- 25
↓	RSH ¹ steel:	+/- 15
↓	Ti alloys:	+/- 10
↓	Nickel based alloys:	+/- 13

Explanations

- v_o = Basic start cutting speed
- v_c = Actual cutting speed
- 1 = Stainless, resistant to heat and acid
- = Temperature in the cutting zone

Feed per Tooth According to Tooth Load Areas

1 Feed per tooth / basic calculation

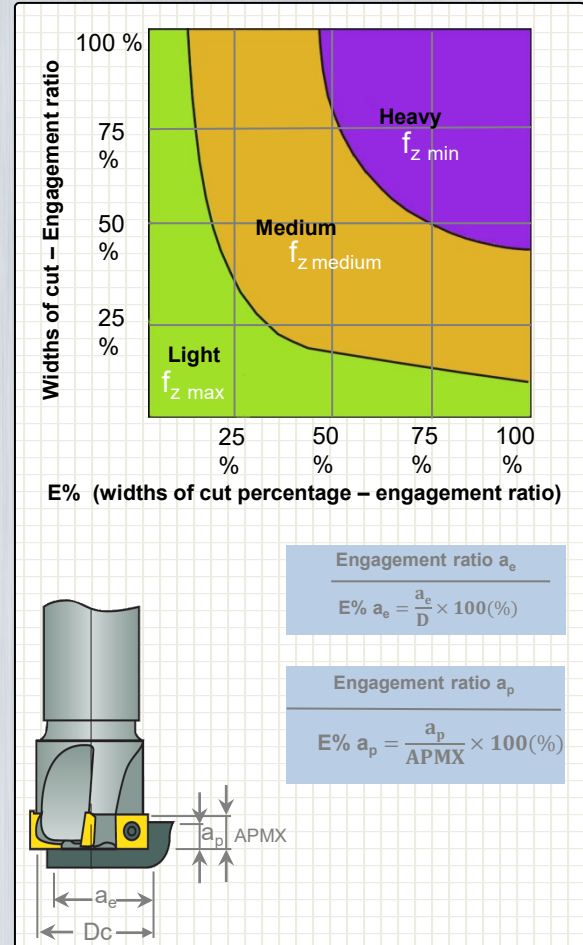
Material		Tensile Strength [N/mm ²]	Hardness HB	HM390-05
				TPKT...PDR
Non-alloy steel and cast steel, free cutting steel	< 0.25 %C	420	125	0.10-0.12-0.15
	>= 0.25 %C	650	190	
	< 0.55 %C	850	250	
	>= 0.55 %C	750	220	
Low alloy steel and cast steel (less than 5% of alloying elements)		1000	300	0.08-0.11-0.14
		600	200	
		930	275	
		1000	300	
		1200	350	0.08-0.10-0.13

First of all, specify the load

Example:
light machining
= maximum
feed per tooth

Please refer to values from the tables on the left

= $f_{z \text{ min}}$
 = $f_{z \text{ medium}}$
 = $f_{z \text{ max}}$



2 f_z -corrective value for long overhang tools

Correction factor for various tool lengths					
Overhang ratio	up to 1 x D	up to 2 x D	up to 3 x D	up to 4 x D	up to 5 x D
Factor	1,00	0,95	0,85	0,75	0,65

$f_z =$ Basic feed per tooth * corrective value, overhang

1

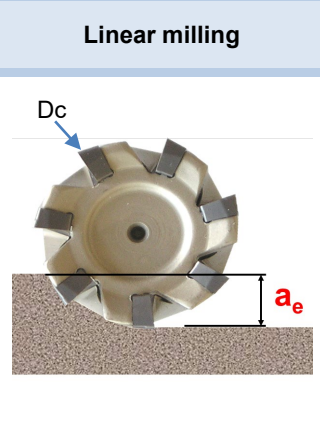
2

Corrective value does not apply to high feed milling cutters.

Feed per Tooth Calculation

According to Radial Depth of Cut a_e

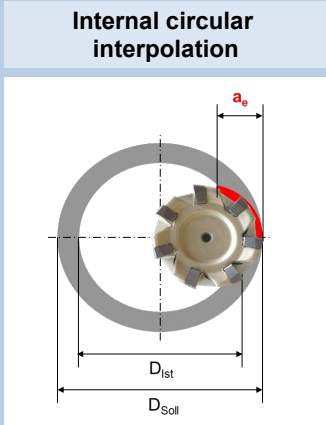
$$a_e = \frac{D_{ist}^2 - D_{soll}^2}{4 \cdot (D_{soll} + D_c)}$$



radial depth = a_e

Eingriffsverhältnis

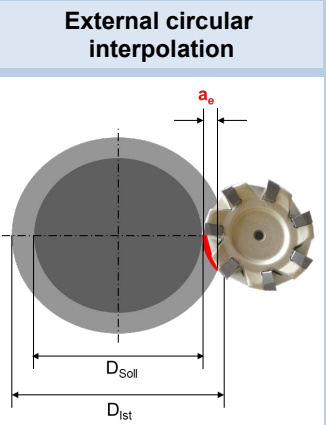
$$E = \frac{a_e}{D_c} \times 100\%$$



$$a_e = \frac{D_{soll}^2 - D_{ist}^2}{4 \times (D_{soll} - D_c)}$$

mittlere Spandicke

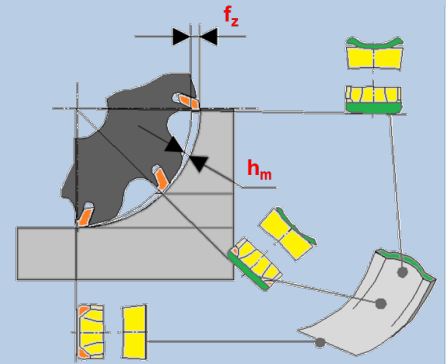
$$h_m = f_z \times \sqrt{a_e / D_c}$$



$$a_e = \frac{D_{ist}^2 - D_{soll}^2}{4 \times (D_{soll} + D_c)}$$

Vorschub pro Zahn

$$f_z = h_m \times \sqrt{D_c / a_e}$$



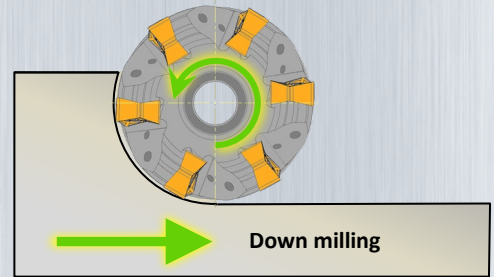
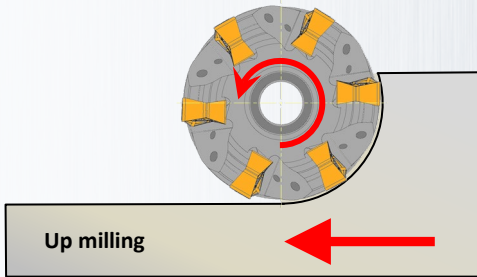
Info:

Only if the tooth feed is correctly calculated and set does the chip formation (constriction) required by the cutting geometry take place.

If the f_z values are too low, they promote premature wear and can cause the chips to jam.

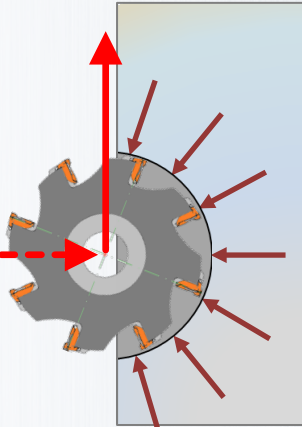
If the f_z values are too high, the cutting inserts will break due to overloading.

Milling Strategies for Optimal Toollife and Machining Process



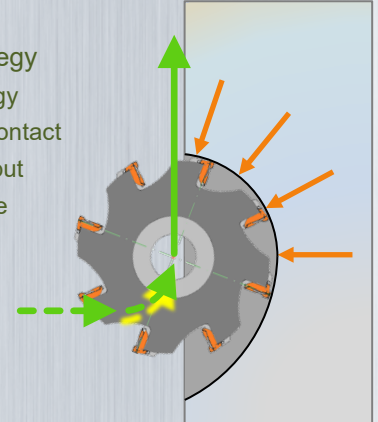
Unfavorable penetration strategy

- Long arc of engagement in cut
- Too many teeth in contact
- High energy input
- Risk of vibrations



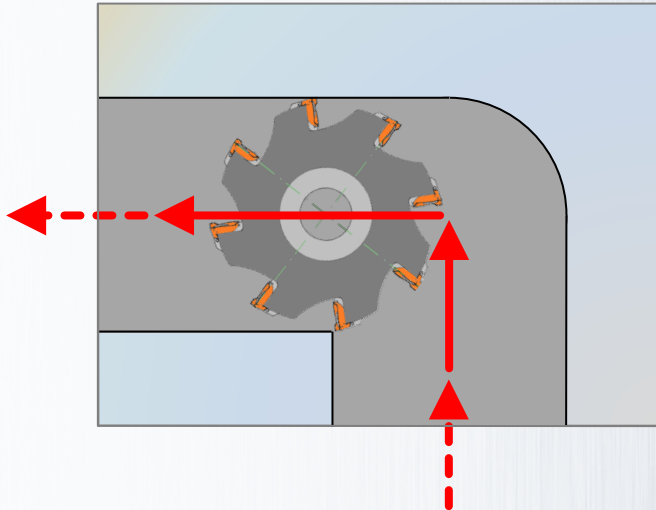
Favorable penetration strategy

- „Roll-In“ strategy
- Less teeth in contact
- Low energy input
- Safe and stable process

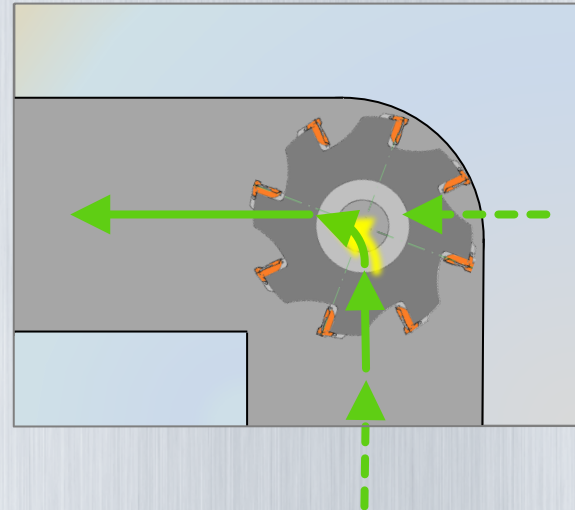


Milling Strategies for Optimal Toollife and Machining Process

Without bottom radius in the edge,
unfavorable



With bottom radius in the edge,
favorable



At internal edge radius,
programming always with roll-in
strategy!

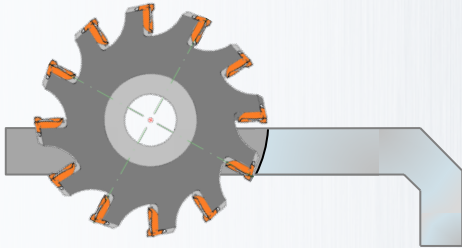
Remark:

Entering the material with 50 % of feed until minimum 2 teeth are constantly in contact.

Exit from material with 50 % of feed in order to avoid hooking and insert breakage.

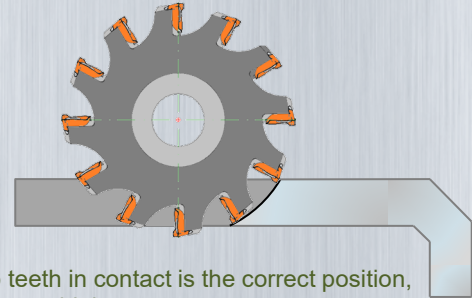
Milling Strategies for Optimal Toollife and Machining Process

Unfavorable Conditions



One tooth in contact, high risk of hooking, tends to chatter.

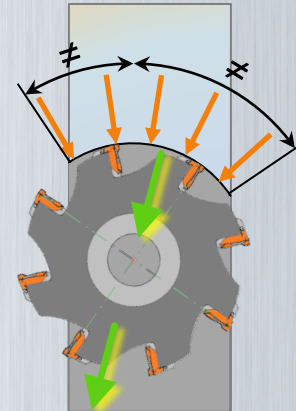
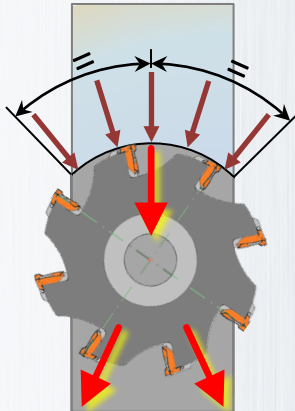
Good conditions, stable process



Two teeth in contact is the correct position, calm machining.

Unfavorable tool position

- No resulting direction of radial force
- Tends to vibrate!

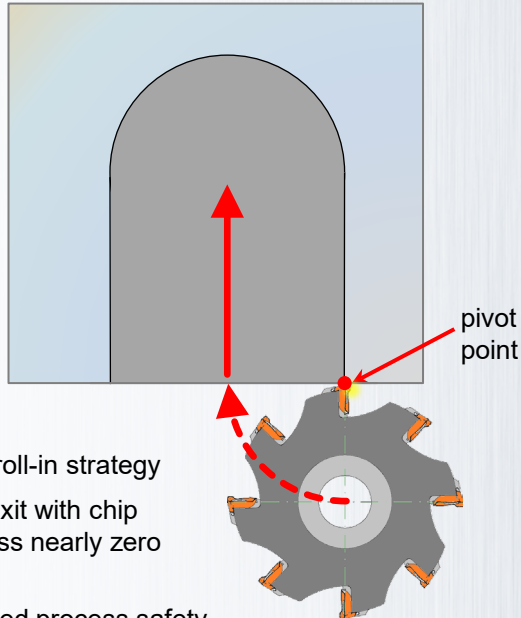


Good tool position

- Resulting direction of radial force
- Little load at material exit (thin chip)

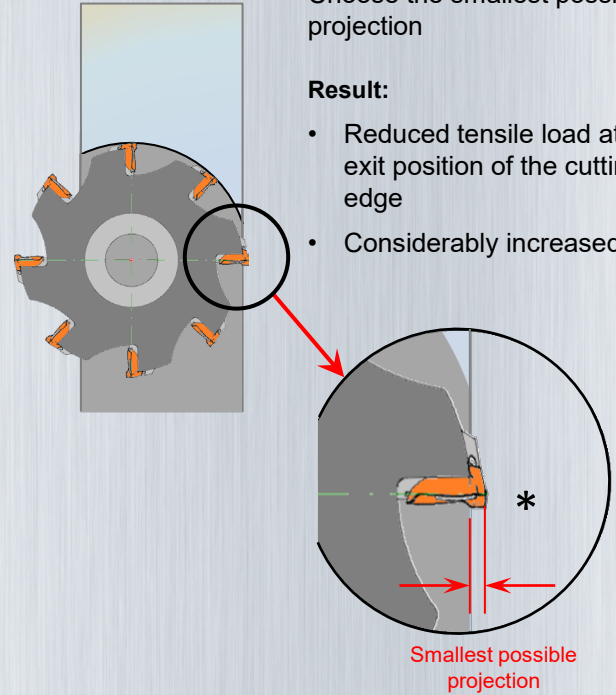
Milling Strategies for Optimal Toollife and Machining Process

Super Alloys and Difficult to Machine Workpiece Materials



Milling by roll-in strategy

- Insert exit with chip thickness nearly zero [mm]
- Increased process safety and toollife
- ISO programming in G3 command



Action:

Choose the smallest possible projection

Result:


- Reduced tensile load at the exit position of the cutting edge
- Considerably increased toollife

* Caution:


Please pay attention to corner radius

Chip formation and Geometries Required According to Workpiece Materials


Nonferrous materials

Non ferrous	Machining process	Geometry required
	<ul style="list-style-type: none"> • mostly long chipping • poor chip control • low temperature 	<ul style="list-style-type: none"> • high positive rake angle • sharp cutting edge • uncoated: with PCD


Cast materials

Cast	Machining process	Geometry required
	<ul style="list-style-type: none"> • very short chipping • good chip breaking • low temperature 	<ul style="list-style-type: none"> • rake angle 0° - 10° • big land • big layer thickness


Non alloy and high alloy steel

Steel	Machining process	Geometry required
	<ul style="list-style-type: none"> • mostly long chipping • chip breaking okay • medium temperature 	<ul style="list-style-type: none"> • positive rake angle • small land • medium layer thickness


Stainless steel

Stainl. steel	Machining process	Geometry required
	<ul style="list-style-type: none"> • lamellar chip • poor chip control • high temperature 	<ul style="list-style-type: none"> • positive rake angle • small honing • little layer thickness

Super alloys and titanium

Super alloys	Machining process	Geometry required
	<ul style="list-style-type: none"> • discontinuous chip • strain hardening • very high temperature 	<ul style="list-style-type: none"> • positive rake angle • ultra fine grade • smooth coating

Hardened steel

Hardened	Machining Process	Geometry required
	<ul style="list-style-type: none"> • short crumbled chips • high power consumption • very high temperature 	<ul style="list-style-type: none"> • negative rake angle • very big wedge angle • big land: CBN

Wear

Wear never occurs as individual appearance but always occurs in various combinations. Therefore, it is essential to monitor the tool's insert soonest possible in order to detect the main wear type and to take counter action accordingly.

Type of wear	Flank wear	Crater wear	Notch wear	Chipping
Reason	<ul style="list-style-type: none">• Cutting speed too high• Temperature too high• Wear resistance of carbide grade not sufficient	<ul style="list-style-type: none">• Cutting speed too high• Temperature too high• Insufficient feed	<ul style="list-style-type: none">• Cutting speed too high• Wear resistance of carbide grade not sufficient	<ul style="list-style-type: none">• Wear resistance of carbide grade too strong• Cutting edge too positive• Build-up edge
Help	<ul style="list-style-type: none">• Reduce cutting speed• Choose more wear resistant carbide grade• Choose reduced lead angle	<ul style="list-style-type: none">• Reduce cutting speed• Choose harder carbide grade• Increase feed	<ul style="list-style-type: none">• Reduce cutting speed• Choose more wear resistant carbide grade• Variable depth of cut	<ul style="list-style-type: none">• Choose tougher carbide grade• Increase cutting speed• Choose more stable cutting edge

Important:

When adjusting or correcting the cutting parameters, we recommend to change the parameters one after another, (not several ones at the same time). To change the cutting conditions by 10 % -20 % (according to workpiece material).

Wear

Wear never occurs as individual appearance but always occurs in various combinations. Therefore, it is essential to monitor the tool's insert soonest possible in order to detect the main wear type and to take counter action accordingly.

Type of wear	Breakage	Thermal cracks	Build-up-edge	Plastic deformation
Reason	<ul style="list-style-type: none">• Cutting edge too positive• Carbide grade too hard• Vibrations	<ul style="list-style-type: none">• Various thermal stress• Strongly interrupted cut• Thermal cracks by coolant	<ul style="list-style-type: none">• Low cutting speed• Feed too low• Cutting edge too negative	<ul style="list-style-type: none">• Feed too high• Cutting speed too high• Carbide grade too tough
Help	<ul style="list-style-type: none">• Reduce depth of cut• Reduce feed• Choose a more stable wedge	<ul style="list-style-type: none">• Choose tougher carbide grade• Improve coolant supply• Dry machining	<ul style="list-style-type: none">• Increase cutting speed• Increase feed• Smooth, positive cutting edge	<ul style="list-style-type: none">• Reduce cutting speed• Reduce feed• Choose harder carbide grade

Important:

When adjusting or correcting the cutting parameters, we recommend to change the parameters one after another, (not several ones at the same time). To change the cutting conditions by 10 % -20 % (according workpiece material).

General recommendations for insert milling

- ✓ Down-milling is to be preferred as the first choice - especially for shoulder milling due to the 90° setting angle.
- ✓ The milling strategy should be chosen so that the cutting forces are directed towards the support points of the clamping device; up-milling can be advantageous in some cases (Figure 1).
- ✓ The strategy regarding the positioning of the milling cutter on the component is of the utmost importance; planning in this regard should be carried out in great detail.
- ✓ For components that are clamped on a clamping tower, 90° milling cutters with a positive insert basic shape (HM390) are recommended. A wide cutter pitch can significantly improve machining, even with negative systems. In any case, the forces should be directed towards the machine bed (Figure 2). We advise against systems with an adjustment angle $< 90^\circ$ due to the higher axial force influence component.
- ✓ The choice of milling pitch should also depend on the stability of the entire system (machine, workpiece clamping, workpiece material, etc.)
- ✓ For SK40 and smaller machines, cutters with a wider pitch are recommended due to the limited stability.

Figure 1

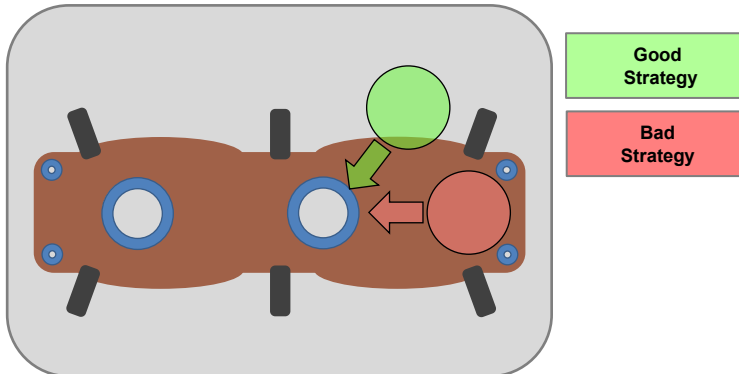
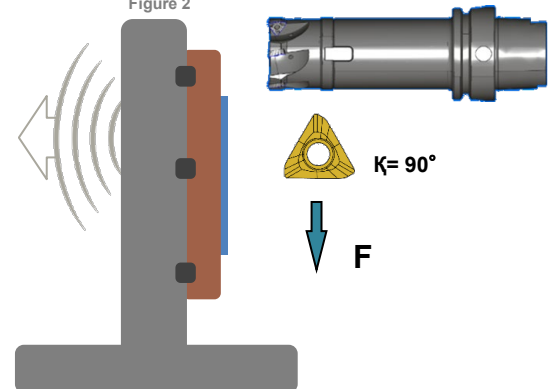
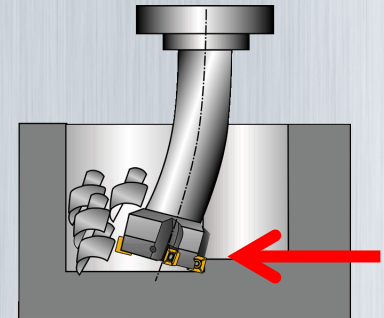
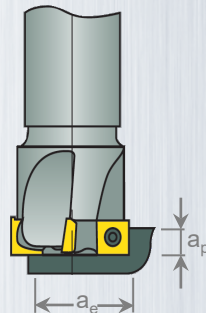
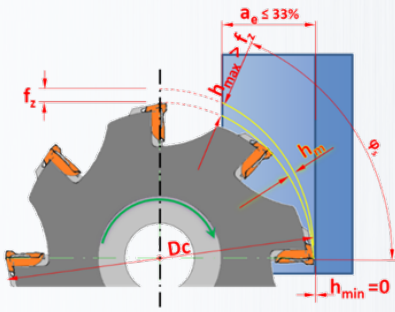


Figure 2



General recommendations for insert milling

- ✓ For the highest possible wall quality, we recommend a cutting depth that is less than 75% of the cutting edge length.
- ✓ For shoulder milling, we recommend starting with a tougher type of carbide than for face milling.
- ✓ When using extended flute cutters, the conditions are often very demanding, so we recommend starting with the toughest grade available, which is recommended for the respective ISO workpiece material range.
- ✓ To avoid vibrations: the deeper the cut, the lower the cutting speed should be. v_c can be chosen.
- ✓ If vibrations occur, we recommend as a first step to reduce the cutting speed v_c and increase the feed f_z to an acceptable range and pay attention to the recommended chip thickness.
- ✓ As a first choice, we recommend using ground inserts. The cutting pressure is lower due to the smaller cutting edge honing.
- ✓ Up-milling can also help stabilize the tool.
- ✓ Make sure that the required machine power is available for the selected cutting values and that the permissible bending moment is not exceeded.
- ✓ Use the ISCAR Machining Power program for this. <https://mpwr.iscar.com/>



Problems and Troubleshooting

TIPS & TRICKS



Problem

Vibrations
on tool

Reason

- Feed insufficient
- Tool diameter too small
- Instable tool clamping
- Insufficient number of teeth in contact
- Minor cutting-edge pushes

Troubleshooting

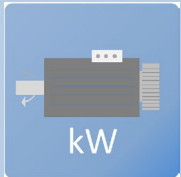
- Increase feed
- Reduce tool overhang
- Improve tool clamping
- Use tool with fine tooth pitch
- Choose a shorter minor cutting edge
- Reduce lead angle



Vibrations
on workpiece

- Instable workpiece clamping
- Instable tool
- Instable tool clamping
- Insufficient number of teeth in contact
- Minor cutting-edge pushes

- Improve general clamping situation
- Cutting force towards stopper
- Reduce axial cutting forces
- Reduce radial cutting force
- Choose a shorter minor cutting edge
- Choose more positive insert
- Choose cutter with coarse tooth pitch



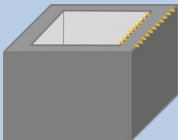
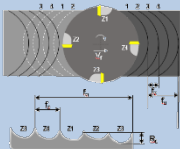
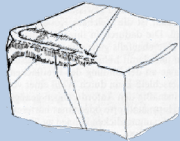
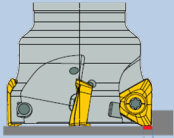
Drive power

- Insufficient machine power
- Metal removal rate too high
- Insert too negative

- Reduce depth of cut
- Reduce width of cut
- Reduce feed per tooth
- Reduce radial cutting force
- Reduce Z_{eff}
- Choose more positive insert

Problems and Troubleshooting

TIPS & TRICKS



Problem	Reason	Troubleshooting
<p>Poor surface quality</p>	<ul style="list-style-type: none"> • Poor axial runout of cutter • Poor radial runout of cutter • Poor radial runout of spindle • Minor cutting edge too small 	<ul style="list-style-type: none"> • Adjust axial runout • Check spindle runout • Check spindle surface • Check precision of toolholder • Choose an insert with wiper edge • Feed per revolution = max. 75 % of minor cutting edge
<p>Tool wear</p>	<p>Please refer to „Types of Wear And Help“</p>	<p>Please refer to „Types of Wear and Help“</p>
<p>Re-cut on second side</p>	<ul style="list-style-type: none"> • Radial cutting forces too high • Cutter vibrates • Cutter diameter too big • Spindle inclination 	<ul style="list-style-type: none"> • Reduce depth of cut • Work with spindle inclination • Check position of wiper insert
<p>Breakages on workpiece</p>	<ul style="list-style-type: none"> • Worn cutting edge • Insert too negative • Increased feed per tooth • High chip thickness at exit • Poor radial runout 	<ul style="list-style-type: none"> • Choose cutter with very fine tooth pitch • Reduce lead angle • Reduce chip cross section • Choose sharper cutting edge • Soft exit from material

Problems and Troubleshooting

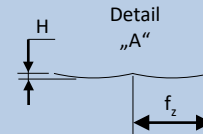
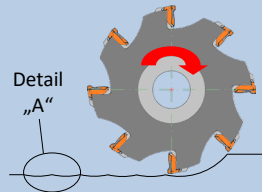
TIPS & TRICKS



Problem	Reason	Troubleshooting
Insufficient chip evacuation	<ul style="list-style-type: none"> • Depth of cut too big • Working angle too big • Chip gullet too small 	<ul style="list-style-type: none"> • Reduce depth of cut • Reduce width of cut • Reduce feed per tooth • Reduce Z_{eff}. • Choose more positive insert
Deformation of arbor Fretting corrosion by micro movements	<ul style="list-style-type: none"> • Adaptation too small • Depth of cut too big • Feed per tooth too big • Feather key not hardened 	<ul style="list-style-type: none"> • Choose bigger adaptation • Reduce Z_{eff}. • Reduce feed per tooth • Reduce depth of cut

Surface geometry – shoulder milling

$$H = \frac{f_z^2}{4 \times D_{tool}}$$



General Formulas

Cutting speed

$$v_c = \frac{Dc \cdot \pi \cdot n}{1000} \text{ [m/min]}$$

Feed per tooth

$$f_z = \frac{v_f}{n \cdot z} \text{ [mm]}$$

Engagement ratio

$$E = \frac{a_e}{Dc} \cdot 100\%$$

RPM

$$n = \frac{v_c \cdot 1000}{Dc \cdot \pi} \text{ [mm}^{-1}\text{]}$$

Feed

$$v_f = f_z \cdot Z \cdot n \text{ [mm/min]}$$

Medium chip thickness

$$h_m = f_z \cdot \sqrt{a_e/Dc}$$

Explanations:

Dc = Tool diameter
z = Number of effective c.e.

v_c = Cutting speed
n = RPM of tool
f_z = Feed per tooth
v_f = Feed

a_e = Cutting width (radial)
a_p = Depth of cut (axial)

E = Engagement ratio (%)
h_m = Medium chip thickness

l = Cutting length
i = Number of passes
Q = Metal removal rate
t_p = Main period of use

π = Pi (3,1415...)

Metal removal rate

$$Q = \frac{a_e \cdot a_p \cdot v_f}{1000} \text{ [cm}^3\text{/min]}$$

Inserts needed for quantity ordered X

$$= \frac{\text{Workpiece} \cdot \text{number of teeth} \cdot \text{production days/month}}{\text{Toolife number of c. e./insert}}$$

Time of engagement

$$t_h = \frac{L \cdot i}{v_f} \text{ [min]}$$

Cutting grade costs per workpiece

$$= \frac{\frac{\text{Cost}}{\text{Insert}} \cdot \text{number of pockets}}{\text{Number of cutting edges/insert} \cdot \text{toolife}}$$

Number of pieces per cutting edge

$$= \frac{\text{Toolife (in min.)} \cdot 60}{\text{Time of engagement/workpiece (in sec.)}}$$

Empirical Formulas for Theoretical Power Consumption

Calculation of performance and torque for cutting parameters review

Steel up to 1000 N/mm²
(GGG50/60)

Cast

Aluminum alloys

Torque calculation

Performance

$$P_{nutz} = \frac{a_p \cdot a_e \cdot v_f}{24.000} \text{ [kW]}$$

Performance

$$P_{nutz} = \frac{a_p \cdot a_e \cdot v_f}{30.000} \text{ [kW]}$$

Performance

$$P_{nutz} = \frac{a_p \cdot a_e \cdot v_f}{60.000} \text{ [kW]}$$

Performance

$$M = 9550 \cdot \frac{P_{nutz}}{n} \text{ [Nm]}$$

Remark:

Performance and torque should be calculated before starting the machining process. By calculating these two parameters, one will be in the position to avoid later tool or machine damage. Just compare the performance and torque chart of the machine tool with the parameters calculated.

Important:

Only if both of these parameters are within the machine tool's performance and torque curve available, a metal cutting process with the metal removal rate calculated will be possible.



You can also carry out all calculations on the ISCAR Machining Power Tool. <https://mpwr.iscar.com>



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